

APPENDICES

Fault finding chart

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Fault finding chart

Fault	Possible cause	Remedy
Metal squirting between matrix and mould.	Worn or damaged matrix. Seating face of mould not level.	Renew matrix. Dismantle mould and re-assemble correctly, ensuring matrix seating face is level.
	Matrix incorrectly inserted in holder. Incorrect adjustment of composition matrix head. 14-36 pt matrix (0.050 drive) in use with holder for 42-72 pt matrix (0.065 drive).	Remove and insert correctly. (Refer to Chapter 19.) Re-adjust. (Refer to 11.1.) Ensure that correct matrix holder is in use.
Metal squirting between nozzle and mould.	Nozzle not rising exactly in the centre of its seating in the mould base.	Centralise the nozzle (refer to 15.7); replace if badly worn or damaged.
	Incorrect engagement of nozzle seating device. Nozzle seating damaged.	Device should be out of action at speeds above 15 r.p.m. Works repair.
Marked or damaged type or type turning in channel.	Type clamp distorted.	Remove clamp and correct distortion.
	Incorrect stroke of type carrier.	Re-adjust. (Refer to 10.5.) Ensure type support spring cam is being used with or without bracket and/or packing, as necessary. (Refer to 10.9.) Check adjustment of type pusher. (Refer to 10.14.) Ensure that type channel blocks are not damaged on type delivery faces.
Stop casting.	Type metal below recommended working temperature.	Adjust temperature. (Refer to Product Information Table.)
	Too much water passing through mould.	Adjust water flow. (Refer to Product Information Table.)
	Blocked nozzle.	Drill nozzle.
	Machine running too slowly.	Adjust speed. (Refer to 15.32.)
	Hole in pump body hat valve obstructed. Incorrect adjustment of the piston operating rod crosshead stud.	Clear obstruction. Re-adjust. (Refer to 15.15.)
Furniture being cast to irregular lengths.	5-em gag not functioning correctly.	Clean and ensure free operation.
	Counter mechanism not registering correctly.	Check adjustment. (Refer to 13.2.)
	Slight compression is not being obtained at mould blade slide drive lever when a non-fusing cast is required. Mould clamp not holding product in position during casting period.	Re-adjust. (Refer to 9.16.) Re-adjust. (Refer to 40.17.)
Inconsistent set size when casting type.	Mould blade coupling fork pin loose.	Tighten by means of knurled nut, and lock in position.
	Micrometer wedge not secured by lock clamps.	Remove clamps and replace, ensuring they are correctly located.
	Mould blade binding. Wedge screw nut damaged.	Dismantle mould, clean and re-assemble. Replace with new nut.
Counter mechanism not registering correctly.	Pawl spring has become disengaged. Counter mechanism out of adjustment.	Re-engage. Re-adjust. (Refer to 13.2.)
Mould blade slide drive lever continually locking.	Mould blade obstructed.	Remove obstruction. (Refer to 9.10.) Ensure friction plunger is sufficiently lubricated.
Type carrier cam lever continually locking.	Obstruction in the path of the type carrier.	Remove obstruction. (Refer to 10.4.)

Speed change table

For display matrices for Super casters equipped with Varigear

Matrix marking	r.p.m. for								
	72pt	60pt	48pt	42pt	36pt	30pt	24pt	18pt	14pt
2	70	85	105	105	140	140	140	145	145
2½	70	85	105	105	140	140	140	145	145
3	70	70	100	100	140	140	140	140	145
3½	55	70	95	100	140	140	140	140	145
4	55	70	85	90	125	135	140	140	145
4½	50	70	85	85	105	125	135	140	145
5	45	60	70	75	105	115	130	140	145
5½	45	55	65	70	90	100	120	135	145
6	40	45	55	60	85	95	120	135	145
6½	40	45	50	55	85	90	115	135	140
7	40	45	50	50	70	90	105	120	140
7½	35	40	45	45	70	85	95	120	135
8	35	40	45	45	55	75	90	110	135
8½	35	35	40	45	55	70	90	105	130
9	30	35	40	45	55	70	85	100	130
9½	30	35	35	40	50	70	80	95	125
10	30	30	35	40	50	65	75	90	125
10½	30	30	35	40	45	55	70	80	110
11	25	30	30	35	45	55	70	80	110
11½	25	25	30	35	40	50	70	75	105
12	22	25	30	35	35	45	55	70	95
13	22	25	30	30	35	40	55	65	90
14	20	22	25	30	30	35	45	60	85
15	18	20	25	25	30	35	45	60	85
16	18	20	22	25	25	30	45	55	85
17	18	18	22	25	25	30	45	55	80
18	15	18	22	25	25	30	40	50	70
19	15	18	18	22	22	25	40	50	70
20	15	18	18	20	20	25	35	50	60
21	15	15	15	18	18	22	30	45	55
22	15	15	15	18	18	20	25	40	50
23	15	15	15	18	18	20	25	35	45
24	15	15	15	18	18	20	25	30	45
25	12	15	15	15	18	20	22	30	45
26	11	15	15	15	15	18	22	25	40
27	10	12	12	15	15	18	22	25	40
28	10	12	12	15	12	15	20	25	35
30	10	12	12	15	12	15	18	20	35
33	8	10	10	12	10	12	18		
36	7	8	9	10	8	12	15		
42	6	7	8	9	5	10			
48	5	6	7	8	5				
54	4	4	6	7					
60	3	4	5	6					
66	3	3	5	5					
72	3	3							
84	2	3							
90	2	2							

Change speed table

Based upon direct drive speed of 144 revolutions per minute

Present matrix marking	Old matrix marking	42 pt to 72 pt (cored)					36 pt and below					
		72	60	54	48	42	36	30	24	18	14	12
2	△ 6 8	†AD 125	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144
2½	△ 7 4 * 2 4	†BD 102	†AD 125	†AD 125	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144
3	△ 7 8 * 2 8	†CD 83	†BD 102	†BD 102	†AD 125	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144
3½	△ 8 4 * 3 4	†AE 68	†CD 83	†BD 102	†BD 102	†AD 125	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144
4	△ 8 8 * 3 8	†BE 55	†AE 68	†CD 83	†CD 83	†BD 102	†AD 125	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144
4½	△ 9 4 * 4 4	†BE 55	†AE 68	†AE 68	†CD 83	†CD 83	†BD 102	†AD 125	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144
5	△ 9 8 * 4 8	†CE 45	†AE 68	†AE 68	†AE 68	†CD 83	†BD 102	†AD 125	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144
5½	△ 10 4 * 5 4	†CE 45	†BE 55	†BE 55	†AE 68	†AE 68	†CD 83	†BD 102	2-H-4 144	2-H-4 144	2-H-4 144	2-H-4 144
6	△ 10 8 * 5 8	†AF 37	†CE 45	†BE 55	†BE 55	†AE 68	†CD 83	†CD 83	†AD 125	2-H-4 144	2-H-4 144	2-H-4 144
6½	△ 11 4 * 6 4	†AF 37	†CE 45	†CE 45	†BE 55	†BE 55	†CD 83	†CD 83	†AD 125	2-H-4 144	2-H-4 144	2-H-4 144
7	△ 11 8 * 6 8	†AF 37	†CE 45	†CE 45	†BE 55	†BE 55	†AE 68	†CD 83	†CD 83	2-H-4 144	2-H-4 144	2-H-4 144
7½	△ 12 4 * 7 4	†BF 30	†AF 37	†CE 45	†CE 45	†BE 55	†AE 68	†CD 83	†CD 83	2-H-4 144	2-H-4 144	2-H-4 144
8	△ 12 8 * 7 8	†BF 30	†AF 37	†AF 37	†CE 45	†BE 55	†BE 55	†AE 68	†CD 83	†BD 102	2-H-4 144	2-H-4 144
8½	△ 13 4 * 8 4	†BF 30	†AF 37	†AF 37	†CE 45	†CE 45	†BE 55	†AE 68	†CD 83	†BD 102	2-H-4 144	2-H-4 144
9	△ 13 8 * 8 8	†CF 25	†BF 30	†AF 37	†CE 45	†CE 45	†BE 55	†AE 68	†CD 83	†BD 102	2-H-4 144	2-H-4 144
9½	△ 14 4 * 9 4	†CF 25	†BF 30	†BF 30	†AF 37	†CE 45	†CE 45	†BE 55	†AE 68	†CD 83	†AD 125	2-H-4 144
10	△ 14 8 * 9 8	†CF 25	†BF 30	†BF 30	†AF 37	†AF 37	†CE 45	†BE 55	†AE 68	†CD 83	†AD 125	2-H-4 144
10½	△ 15 4 * 10 4	†CF 25	†CF 25	†BF 30	†BF 30	†AF 37	†CE 45	†CE 45	†AE 68	†CD 83	†BD 102	†AD 125
11	△ 15 8 * 10 8	†AD 22	†CF 25	†BF 30	†BF 30	†AF 37	†CE 45	†CE 45	†AE 68	†CD 83	†BD 102	†AD 125
11½	△ 16 4 * 11 4	†AD 22	†CF 25	†BF 30	†BF 30	†AF 37	†CE 45	†CE 45	†AE 68	†CD 83	†BD 102	†AD 125
12	△ 16 8 * 11 8	†AD 22	†CF 25	†CF 25	†BF 30	†AF 37	†AF 37	†CE 45	†BE 55	†CD 83	†CD 83	†BD 102
13	△ 17 8 * 12 8	†BD 18	†AD 22	†CF 25	†BF 30	†BF 30	†AF 37	†CE 45	†BE 55	†CD 83	†CD 83	†BD 102
14	△ 18 8 * 13 8	†BD 18	†AD 22	†AD 22	†CF 25	†BF 30	†BF 30	†AF 37	†CE 45	†AE 68	†CD 83	†CD 83
15	* 2 8 * 14 8	†CD 15	†BD 18	†AD 22	†CF 25	†CF 25	†BF 30	†AF 37	†CE 45	†AE 68	†CD 83	†CD 83

Present matrix marking	Old matrix marking	42 pt to 72 pt (cored)					36 pt and below					
		72	60	54	48	42	36	30	24	18	14	12
16	* 3 8 * 15 8	†CD	†BD	†AD	†AD	†CF	†CF	†BF	†CE	†BE	†CD	†CD
17	* 4 8 * 16 8	†CD	†BD	†BD	†AD	†CF	†CF	†BF	†CE	†BE	†CD	†CD
18	* 5 8 * 17 8	†AE	†CD	†BD	†AD	†AD	†AD	†CF	†AF	†CE	†AE	†CD
19	* 6 8 * 18 8	†AE	†CD	†CD	†BD	†AD	†AD	†CF	†AF	†CE	†AE	†CD
20	* 7 8 2 8	†AE	†CD	†CD	†BD	†AD	†BD	†AD	†BF	†CE	†BE	†AE
21	* 8 8 3 8	†AE	†AE	†CD	†CD	†BD	†BD	†AD	†BF	†CE	†BE	†AE
22	* 9 8 4 8	†BE	†AE	†CD	†CD	†BD	†BD	†BD	†CF	†AF	†CE	†BE
23	* 10 8 5 8	†BE	†AE	†CD	†CD	†BD	†BD	†BD	†CF	†AF	†CE	†BE
24	* 11 8 6 8	†BE	†AE	†AE	†CD	†BD	†BD	†BD	†CF	†AF	†CE	†BE
25	* 12 8 7 8	†BE	†BE	†BE	†CD	†CD	†CD	†BD	†AD	†BF	†CE	
26	* 13 8 8 8	†BE	†BE	†BE	†CD	†CD	†CD	†BD	†AD	†BF	†CE	
27	* 14 8 9 8	†CE	†BE	†BE	†AE	†CD	†CD	†BD	†AD	†BF	†CE	
28	* 15 8 10 8	†CE	†BE	†BE	†AE	†CD	†AE	†CD	†BD	†CF	†AF	
30	* 17 8 12 8	†CE	†BE	†BE	†AE	†CD	†AE	†CD	†BD	†CF	†AF	
33	3 8 15 8	†AF	†CE	†BE	†BE	†AE	†BE	†AE	†BD			
36	6 8 18 8	†AF	†CE	†BE	†BE	†BE	†CE	†AE	†CD			
42	12 8 ** 7 8	†BF	†AF	†CE	†CE	†CE	†BE	†BE				
48	18 8 ** 13 8	†CF	†BF	†AF	†AF	†CE	†CF					
54		§†CE	†CF	†BF	†BF	†AF						
60		§†CE	†CF	†CF	†BF	†AF						
66		§†AF	§†CE	†CF	†CF	†BF						
72		§†BF	§†CE									
84		§†BF	§†AF									
90		§†CF	§†CF									

† These have speed control 1-3-H in operation ‡ These have speed control 2-3-G in operation § Pump to be stopped every alternate revolution

Counter drum and micrometer head settings

Table showing adjustments in pica ems and half-emms, for use with furniture mould equipped for casting predetermined lengths.

Adjustments				Adjustments				Adjustments				Adjustments			
Pica ems	Drum (casts)	Indicator scale (ems)	Micrometer wedge +	Pica ems	Drum (casts)	Indicator scale (ems)	Micrometer wedge +	Pica ems	Drum (casts)	Indicator scale (ems)	Micrometer wedge +	Pica ems	Drum (casts)	Indicator scale (ems)	Micrometer wedge +
8	1	3		27	4	5½		46	7	5½	0.0592	65	10	6	
8½	1	3½		27½	4	5½	0.0207	46½	7	5½	0.0711	65½	11	5½	
9	1	4		28	4	5½	0.0415	47	7	6		66	11	5½	0.0075
9½	1	4½		28½	4	5½	0.0622	47½	8	5	0.0519	66½	11	5½	0.0151
10	1	5		29	4	6		48	8	5	0.0622	67	11	5½	0.0226
10½	1	5½		29½	5	4½	0.0664	48½	8	5	0.0726	67½	11	5½	0.0301
11	1	6		30	5	5		49	8	5½		68	11	5½	0.0377
11½	2	3	0.0415	30½	5	5	0.0166	49½	8	5½	0.0103	68½	11	5½	0.0453
12	2	3½		31	5	5	0.0332	50	9	5		69	11	5½	0.0528
12½	2	3½	0.0415	31½	5	5	0.0498	50½	8	5½	0.0311	69½	11	5½	0.0604
13	2	4		32	5	5	0.0664	51	8	5½	0.0415	70	13	5	
13½	2	4	0.0415	32½	5	5½		51½	8	5½	0.0518	70½	11	5½	0.0754
14	2	4½		33	5	5½	0.0166	52	8	5½	0.0622	71	11	6	
14½	2	4½	0.0415	33½	5	5½	0.0332	52½	8	5½	0.0727	71½	12	5½	0.0069
15	2	5		34	5	5½	0.0498	53	8	6		72	12	5½	0.0138
15½	2	5	0.0415	34½	5	5½	0.0664	53½	9	5	0.0645	72½	12	5½	0.0208
16	2	5½		35	5	6		54	9	5	0.0715	73	12	5½	0.0276
16½	2	5½	0.0415	35½	6	5	0.0138	54½	9	5½		73½	12	5½	0.0345
17	2	6		36	6	5	0.0276	55	10	5		74	12	5½	0.0415
17½	3	4	0.0276	36½	6	5	0.0414	55½	10	5	0.0083	74½	12	5½	0.0484
18	3	4	0.0553	37	6	5	0.0552	56	10	5	0.0166	75	14	5	
18½	3	4½		37½	6	5	0.0691	56½	10	5	0.0249	75½	12	5½	0.0622
19	3	4½	0.0276	38	6	5½		57	9	5½	0.0461	76	12	5½	0.0691
19½	3	4½	0.0553	38½	6	5½	0.0138	57½	9	5½	0.0553	76½	13	5½	
20	3	5		39	6	5½	0.0276	58	9	5½	0.0645	77	12	6	
20½	3	5	0.0276	39½	6	5½	0.0415	58½	9	5½	0.0737	77½	13	5½	0.0127
21	3	5	0.0553	40	7	5		59	9	6		78	13	5½	0.0191
21½	3	5½		40½	6	5½	0.0691	59½	10	5	0.0747	78½	13	5½	0.0255
22	3	5½	0.0276	41	6	6		60	11	5		79	13	5½	0.0319
22½	3	5½	0.0553	41½	7	5	0.0355	60½	10	5½	0.0083	79½	13	5½	0.0383
23	3	6		42	7	5	0.0474	61	10	5½	0.0166	80	15	5	
23½	4	4½	0.0207	42½	7	5	0.0592	61½	10	5½	0.0249	80½	13	5½	0.0511
24	4	4½	0.0415	43	7	5	0.0711	62	10	5½	0.0332	81	13	5½	0.0575
24½	4	4½	0.0622	43½	7	5½		62½	10	5½	0.0415	81½	13	5½	0.0638
25	4	5		44	7	5½	0.0118	63	10	5½	0.0498	82	14	5½	
25½	4	5	0.0207	44½	7	5½	0.0237	63½	10	5½	0.0581	82½	13	5½	0.0766
26	4	5	0.0415	45	8	5		64	10	5½	0.0664	83	13	6	
26½	4	5	0.0622	45½	7	5½	0.0474	64½	10	5½	0.0747	83½	14	5½	0.0178

Pica ems	Adjustments			Pica ems	Adjustments			Pica ems	Adjustments			Pica ems	Adjustments		
	<i>Drum (casts)</i>	<i>Indicator scale (ems)</i>	<i>Micrometer wedge +</i>		<i>Drum (casts)</i>	<i>Indicator scale (ems)</i>	<i>Micrometer wedge +</i>		<i>Drum (casts)</i>	<i>Indicator scale (ems)</i>	<i>Micrometer wedge +</i>		<i>Drum (casts)</i>	<i>Indicator scale (ems)</i>	<i>Micrometer wedge +</i>
84 ^r	14	5½	0.0237	103	17	5½	0.0439	122	20	5½	0.0581	141	23	5½	0.0686
84½	14	5½	0.0296	103½	17	5½	0.0488	122½	20	5½	0.0623	141½	23	5½	0.0722
85	16	5		104	18	5½		123	20	5½	0.0664	142	23	5½	0.0758
85½	14	5½	0.0415	104½	17	5½	0.0586	123½	20	5½	0.0705	142½	25	5½	
86	14	5½	0.0474	105	20	5		124	20	5½	0.0747	143	23	6	
86½	14	5½	0.0534	105½	17	5½	0.0683	124½	20	5½	0.0788	143½	24	5½	0.0450
87	14	5½	0.0593	106	17	5½	0.0732	125	20	6		144	24	5½	0.0484
87½	15	5½		106½	17	5½	0.0781	125½	21	5½	0.0395	144½	24	5½	0.0519
88	14	5½	0.0711	107	17	6		126	22	5½		145	24	5½	0.0554
88½	14	5½	0.0771	107½	18	5½	0.0323	126½	21	5½	0.0474	145½	24	5½	0.0583
89	14	6		108	18	5½	0.0369	127	21	5½	0.0514	146	24	5½	0.0623
89½	15	5½	0.0221	108½	18	5½	0.0415	127½	21	5½	0.0553	146½	24	5½	0.0657
90	17	5		109	18	5½	0.0461	128	21	5½	0.0593	147	24	5½	0.0692
90½	15	5½	0.0332	109½	19	5½		128½	21	5½	0.0632	147½	24	5½	0.0726
91	15	5½	0.0387	110	21	5		129	21	5½	0.0672	148	24	5½	0.0761
91½	15	5½	0.0443	110½	18	5½	0.0599	129½	21	5½	0.0711	148½	24	5½	0.0795
92	15	5½	0.0498	111	18	5½	0.0646	130	25	5		149	24	6	
92½	15	5½	0.0553	111½	18	5½	0.0692	130½	21	5½	0.0790	149½	25	5½	0.0465
93	16	5½		112	18	5½	0.0738	131	21	6		150	25	5½	0.0498
93½	15	5½	0.0664	112½	18	5½	0.0784	131½	23	5½		150½	25	5½	0.0531
94	15	5½	0.0719	113	18	6		132	22	5½	0.0453	151	25	5½	0.0564
94½	15	5½	0.0774	113½	19	5½	0.0349	132½	22	5½	0.0490	151½	25	5½	0.0598
95	15	6		114	19	5½	0.0393	133	22	5½	0.0528	152	25	5½	0.0631
95½	16	5½	0.0259	114½	19	5½	0.0437	133½	22	5½	0.0566	152½	25	5½	0.0664
96	16	5½	0.0311	115	22	5		134	22	5½	0.0603	153	25	5½	0.0697
96½	16	5½	0.0363	115½	19	5½	0.0524	134½	22	5½	0.0641	153½	25	5½	0.0730
97	16	5½	0.0415	116	19	5½	0.0568	135	22	5½	0.0679	154	25	5½	0.0763
97½	16	5½	0.0467	116½	19	5½	0.0612	135½	22	5½	0.0716	154½	25	5½	0.0796
98	16	5½	0.0519	117	19	5½	0.0655	136	22	5½	0.0754	155	25	5½	0.0830
98½	17	5½		117½	19	5½	0.0699	136½	22	5½	0.0792				
99	16	5½	0.0623	118	19	5½	0.0743	137	22	6					
99½	16	5½	0.0675	118½	19	5½	0.0786	137½	23	5½	0.0433				
100	19	5		119	19	6		138	23	5½	0.0469				
100½	16	5½	0.0778	119½	20	5½	0.0374	138½	23	5½	0.0505				
101	16	6		120	23	5		139	23	5½	0.0541				
101½	17	5½	0.0293	120½	21	5½		139½	23	5½	0.0577				
102	17	5½	0.0342	121	20	5½	0.0498	140	23	5½	0.0613				
102½	17	5½	0.0391	121½	20	5½	0.0540	140½	23	5½	0.0650				

Counter drum and micrometer head settings

Table showing adjustments in ciceros and half-ciceros, for use with furniture mould equipped for casting predetermined lengths.

Adjustments				Adjustments				Adjustments				Adjustments							
Ciceros		Drum (casts)	Indicator scale (ems)	Micrometer wedge +	Ciceros		Drum (casts)	Indicator scale (ems)	Micrometer wedge +	Ciceros		Drum (casts)	Indicator scale (ems)	Micrometer wedge +	Ciceros		Drum (casts)	Indicator scale (ems)	Micrometer wedge +
7½	1	3	0.0040	25	4	5	0.0725	43	7	5½	0.0594	61	12	5	0.0038	79	12	5½	0.0204
8	1	3½	0.0098	25½	4	5½	0.0117	43½	7	5½	0.0721	61½	11	5½	0.0080	79½	12	5½	0.0212
8½	1	4	0.0156	26	4	5½	0.0339	44	8	5	0.0431	62	11	5½	0.0161	80	12	5½	0.0220
9	1	4½	0.0214	26½	4	5½	0.0561	44½	8	5	0.0541	62½	11	5½	0.0242	80½	12	5½	0.0228
9½	1	5	0.0272	27	4	5½	0.0788	45	8	5	0.0652	63	11	5½	0.0322	81	12	5½	0.0236
10	1	5½	0.0330	27½	5	4½	0.0638	45½	8	5	0.0763	63½	11	5½	0.0403	81½	12	5½	0.0244
10½	2	3	0.0194	28	5	4½	0.0815	46	8	5½	0.0045	64	11	5½	0.0483	82	12	5½	0.0252
11	2	3	0.0638	28½	5	5	0.0163	46½	8	5½	0.0156	64½	11	5½	0.0564	82½	12	5½	0.0260
11½	2	3½	0.0252	29	5	5	0.0341	47	8	5½	0.0266	65	11	5½	0.0645	83	12	5½	0.0268
12	2	3½	0.0696	29½	5	5	0.0518	47½	8	5½	0.0376	65½	11	5½	0.0726	83½	12	5½	0.0276
12½	2	4	0.0310	30	5	5	0.0696	48	8	5½	0.0489	66	11	5½	0.0807	84	12	5½	0.0284
13	2	4	0.0754	30½	5	5½	0.0044	48½	8	5½	0.0599	66½	12	5½	0.0020	84½	12	5½	0.0292
13½	2	4½	0.0368	31	5	5½	0.0221	49	8	5½	0.0710	67	12	5½	0.0095	85	12	5½	0.0300
14	2	4½	0.0812	31½	5	5½	0.0399	49½	8	5½	0.0821	67½	12	5½	0.0178	85½	12	5½	0.0308
14½	2	5	0.0426	32	5	5½	0.0576	50	9	5	0.0644	68	12	5½	0.0242	86	12	5½	0.0316
15	2	5½	0.0040	32½	5	5½	0.0754	50½	9	5	0.0743	68½	12	5½	0.0317	86½	12	5½	0.0324
15½	2	5½	0.0484	33	6	5	0.0085	51	9	5½	0.0012	69	12	5½	0.0426	87	12	5½	0.0332
16	3	4	0.0065	33½	6	5	0.0233	51½	9	5½	0.0110	69½	12	5½	0.0470	87½	12	5½	0.0340
16½	3	4	0.0361	34	6	5	0.0381	52	9	5½	0.0209	70	12	5½	0.0542	88	12	5½	0.0348
17	3	4	0.0657	34½	6	5	0.0529	52½	9	5½	0.0308	70½	12	5½	0.0612	88½	12	5½	0.0356
17½	3	4½	0.0123	35	6	5	0.0677	53	9	5½	0.0406	71	12	5½	0.0687	89	12	5½	0.0364
18	3	4½	0.0419	35½	6	5	0.0825	53½	9	5½	0.0505	71½	12	5½	0.0760	89½	12	5½	0.0372
18½	3	4½	0.0715	36	6	5½	0.0142	54	9	5½	0.0604	72	13	5½	0.0068	90	12	5½	0.0380
19	3	5	0.0181	36½	6	5½	0.0291	54½	9	5½	0.0702	72½	13	5½	0.0136	90½	12	5½	0.0388
19½	3	5	0.0477	37	6	5½	0.0439	55	9	5½	0.0801	73	13	5½	0.0204	91	12	5½	0.0396
20	3	5	0.0773	37½	6	5½	0.0587	55½	10	5	0.0727	73½	13	5½	0.0273	91½	12	5½	0.0404
20½	3	5½	0.0239	38	6	5½	0.0735	56	10	5	0.0815	74	13	5½	0.0341	92	12	5½	0.0412
21	3	5½	0.0535	38½	7	5	0.0282	56½	10	5½	0.0074	74½	13	5½	0.0409	92½	12	5½	0.0420
21½	4	4½	0.0001	39	7	5	0.0409	57	10	5½	0.0163	75	13	5½	0.0478	93	12	5½	0.0428
22	4	4½	0.0223	39½	7	5	0.0536	57½	10	5½	0.0252	75½	13	5½	0.0546	93½	12	5½	0.0436
22½	4	4½	0.0445	40	7	5	0.0663	58	10	5½	0.0341	76	13	5½	0.0614	94	12	5½	0.0444
23	4	4½	0.0667	40½	7	5	0.0789	58½	10	5½	0.0429	76½	13	5½	0.0683	94½	12	5½	0.0452
23½	4	5	0.0059	41	7	5½	0.0087	59	10	5½	0.0518	77	13	5½	0.0751	95	12	5½	0.0460
24	4	5	0.0281	41½	7	5½	0.0213	59½	10	5½	0.0607	77½	13	5½	0.0817	95½	12	5½	0.0468
24½	4	5	0.0403	42	7	5½	0.0340	60	10	5½	0.0696	78	14	5½	0.0012	96	12	5½	0.0476
				42½	7	5½	0.0467	60½	10	5½	0.0785	78½	14	5½	0.0080	96½	12	5½	0.0484

Adjustments				Adjustments				Adjustments				Adjustments			
Ciceros	Drum (casts)	Indicator scale (ems)	Micrometer wedge +	Ciceros	Drum (casts)	Indicator scale (ems)	Micrometer wedge +	Ciceros	Drum (casts)	Indicator scale (ems)	Micrometer wedge +	Ciceros	Drum (casts)	Indicator scale (ems)	Micrometer wedge +
79	14	5 $\frac{1}{2}$	0.0299	97	17	5 $\frac{1}{2}$	0.0515	115	20	5 $\frac{1}{2}$	0.0667	133	23	5 $\frac{1}{2}$	0.0779
79 $\frac{1}{2}$	14	5 $\frac{1}{2}$	0.0362	97 $\frac{1}{2}$	17	5 $\frac{1}{2}$	0.0568	115 $\frac{1}{2}$	20	5 $\frac{1}{2}$	0.0711	133 $\frac{1}{2}$	23	5 $\frac{1}{2}$	0.0818
80	14	5 $\frac{1}{2}$	0.0424	98	17	5 $\frac{1}{2}$	0.0619	116	20	5 $\frac{1}{2}$	0.0755	134	24	5 $\frac{1}{2}$	0.0440
80 $\frac{1}{2}$	14	5 $\frac{1}{2}$	0.0492	98 $\frac{1}{2}$	17	5 $\frac{1}{2}$	0.0672	116 $\frac{1}{2}$	20	5 $\frac{1}{2}$	0.0800	134 $\frac{1}{2}$	24	5 $\frac{1}{2}$	0.0477
81	14	5 $\frac{1}{2}$	0.0552	99	17	5 $\frac{1}{2}$	0.0724	117	21	5 $\frac{1}{2}$	0.0369	135	24	5 $\frac{1}{2}$	0.0514
81 $\frac{1}{2}$	14	5 $\frac{1}{2}$	0.0616	99 $\frac{1}{2}$	17	5 $\frac{1}{2}$	0.0777	117 $\frac{1}{2}$	21	5 $\frac{1}{2}$	0.0412	135 $\frac{1}{2}$	24	5 $\frac{1}{2}$	0.0551
82	14	5 $\frac{1}{2}$	0.0679	100	18	5 $\frac{1}{2}$	0.0276	118	21	5 $\frac{1}{2}$	0.0454	136	24	5 $\frac{1}{2}$	0.0588
82 $\frac{1}{2}$	14	5 $\frac{1}{2}$	0.0743	100 $\frac{1}{2}$	18	5 $\frac{1}{2}$	0.0325	118 $\frac{1}{2}$	21	5 $\frac{1}{2}$	0.0492	136 $\frac{1}{2}$	24	5 $\frac{1}{2}$	0.0625
83	14	5 $\frac{1}{2}$	0.0806	101	18	5 $\frac{1}{2}$	0.0374	119	21	5 $\frac{1}{2}$	0.0538	137	24	5 $\frac{1}{2}$	0.0662
83 $\frac{1}{2}$	15	5 $\frac{1}{2}$	0.0203	101 $\frac{1}{2}$	18	5 $\frac{1}{2}$	0.0423	119 $\frac{1}{2}$	21	5 $\frac{1}{2}$	0.0577	137 $\frac{1}{2}$	24	5 $\frac{1}{2}$	0.0699
84	15	5 $\frac{1}{2}$	0.0262	102	18	5 $\frac{1}{2}$	0.0473	120	21	5 $\frac{1}{2}$	0.0622	138	24	5 $\frac{1}{2}$	0.0736
84 $\frac{1}{2}$	15	5 $\frac{1}{2}$	0.0321	102 $\frac{1}{2}$	18	5 $\frac{1}{2}$	0.0522	120 $\frac{1}{2}$	21	5 $\frac{1}{2}$	0.0665	138 $\frac{1}{2}$	24	5 $\frac{1}{2}$	0.0773
85	15	5 $\frac{1}{2}$	0.0381	103	18	5 $\frac{1}{2}$	0.0572	121	21	5 $\frac{1}{2}$	0.0708	139	24	5 $\frac{1}{2}$	0.0810
85 $\frac{1}{2}$	15	5 $\frac{1}{2}$	0.0440	103 $\frac{1}{2}$	18	5 $\frac{1}{2}$	0.0621	121 $\frac{1}{2}$	21	5 $\frac{1}{2}$	0.0750	139 $\frac{1}{2}$	25	5 $\frac{1}{2}$	0.0448
86	15	5 $\frac{1}{2}$	0.0499	104	18	5 $\frac{1}{2}$	0.0681	122	21	5 $\frac{1}{2}$	0.0792	140	25	5 $\frac{1}{2}$	0.0484
86 $\frac{1}{2}$	15	5 $\frac{1}{2}$	0.0565	104 $\frac{1}{2}$	18	5 $\frac{1}{2}$	0.0719	122 $\frac{1}{2}$	22	5 $\frac{1}{2}$	0.0382	140 $\frac{1}{2}$	25	5 $\frac{1}{2}$	0.0519
87	15	5 $\frac{1}{2}$	0.0617	105	18	5 $\frac{1}{2}$	0.0766	123	22	5 $\frac{1}{2}$	0.0422	141	25	5 $\frac{1}{2}$	0.0555
87 $\frac{1}{2}$	15	5 $\frac{1}{2}$	0.0677	105 $\frac{1}{2}$	18	5 $\frac{1}{2}$	0.0818	123 $\frac{1}{2}$	22	5 $\frac{1}{2}$	0.0463	141 $\frac{1}{2}$	25	5 $\frac{1}{2}$	0.0590
88	15	5 $\frac{1}{2}$	0.0736	106	19	5 $\frac{1}{2}$	0.0305	124	22	5 $\frac{1}{2}$	0.0503	142	25	5 $\frac{1}{2}$	0.0626
88 $\frac{1}{2}$	15	5 $\frac{1}{2}$	0.0795	106 $\frac{1}{2}$	19	5 $\frac{1}{2}$	0.0409	124 $\frac{1}{2}$	22	5 $\frac{1}{2}$	0.0543	142 $\frac{1}{2}$	25	5 $\frac{1}{2}$	0.0661
89	16	5 $\frac{1}{2}$	0.0230	107	19	5 $\frac{1}{2}$	0.0435	125	22	5 $\frac{1}{2}$	0.0584	143	25	5 $\frac{1}{2}$	0.0697
89 $\frac{1}{2}$	16	5 $\frac{1}{2}$	0.0286	107 $\frac{1}{2}$	19	5 $\frac{1}{2}$	0.0481	125 $\frac{1}{2}$	22	5 $\frac{1}{2}$	0.0624	143 $\frac{1}{2}$	25	5 $\frac{1}{2}$	0.0732
90	16	5 $\frac{1}{2}$	0.0341	108	19	5 $\frac{1}{2}$	0.0528	126	22	5 $\frac{1}{2}$	0.0664	144	25	5 $\frac{1}{2}$	0.0768
90 $\frac{1}{2}$	16	5 $\frac{1}{2}$	0.0397	108 $\frac{1}{2}$	19	5 $\frac{1}{2}$	0.0575	126 $\frac{1}{2}$	22	5 $\frac{1}{2}$	0.0705	144 $\frac{1}{2}$	25	5 $\frac{1}{2}$	0.0803
91	16	5 $\frac{1}{2}$	0.0452	109	19	5 $\frac{1}{2}$	0.0622	127	22	5 $\frac{1}{2}$	0.0745				
91 $\frac{1}{2}$	16	5 $\frac{1}{2}$	0.0508	109 $\frac{1}{2}$	19	5 $\frac{1}{2}$	0.0668	127 $\frac{1}{2}$	22	5 $\frac{1}{2}$	0.0789				
92	16	5 $\frac{1}{2}$	0.0563	110	19	5 $\frac{1}{2}$	0.0715	128	22	5 $\frac{1}{2}$	0.0825				
92 $\frac{1}{2}$	16	5 $\frac{1}{2}$	0.0619	110 $\frac{1}{2}$	19	5 $\frac{1}{2}$	0.0762	128 $\frac{1}{2}$	23	5 $\frac{1}{2}$	0.0432				
93	16	5 $\frac{1}{2}$	0.0674	111	19	5 $\frac{1}{2}$	0.0809	129	23	5 $\frac{1}{2}$	0.0470				
93 $\frac{1}{2}$	16	5 $\frac{1}{2}$	0.0729	111 $\frac{1}{2}$	20	5 $\frac{1}{2}$	0.0356	129 $\frac{1}{2}$	23	5 $\frac{1}{2}$	0.0509				
94	16	5 $\frac{1}{2}$	0.0785	112	20	5 $\frac{1}{2}$	0.0401	130	23	5 $\frac{1}{2}$	0.0547				
94 $\frac{1}{2}$	17	5 $\frac{1}{2}$	0.0254	112 $\frac{1}{2}$	20	5 $\frac{1}{2}$	0.0445	130 $\frac{1}{2}$	23	5 $\frac{1}{2}$	0.0586				
95	17	5 $\frac{1}{2}$	0.0307	113	20	5 $\frac{1}{2}$	0.0489	131	23	5 $\frac{1}{2}$	0.0625				
95 $\frac{1}{2}$	17	5 $\frac{1}{2}$	0.0359	113 $\frac{1}{2}$	20	5 $\frac{1}{2}$	0.0534	131 $\frac{1}{2}$	23	5 $\frac{1}{2}$	0.0663				
96	17	5 $\frac{1}{2}$	0.0411	114	20	5 $\frac{1}{2}$	0.0578	132	23	5 $\frac{1}{2}$	0.0702				
96 $\frac{1}{2}$	17	5 $\frac{1}{2}$	0.0463	114 $\frac{1}{2}$	20	5 $\frac{1}{2}$	0.0622	132 $\frac{1}{2}$	23	5 $\frac{1}{2}$	0.0740				

Cutting strip material (pica ems)

The following table shows the position of the counter drum and the adjustment of the micrometer wedge to shear strip material to pica ems and half-ems

Pica ems	Adjustments			Pica ems	Adjustments			Pica ems	Adjustments			Pica ems	Adjustments		
	Drum (casts)	Indicator scale (ems)	Micrometer wedge +		Drum (casts)	Indicator scale (ems)	Micrometer wedge +		Drum (casts)	Indicator scale (ems)	Micrometer wedge +		Drum (casts)	Indicator scale (ems)	Micrometer wedge +
5	1	5		25	5	5		45	9	5		65	13	5	
5½	1	5½		25½	5	5	0.0166	45½	8	5½	0.0311	65½	11	5½	0.0754
6	1	6		26	5	5	0.0332	46	8	5½	0.0415	66	11	6	
6½	2	3	0.0415	26½	5	5	0.0498	46½	8	5½	0.0518	66½	12	5½	0.0069
7	2	3½		27	5	5	0.0664	47	8	5½	0.0622	67	12	5½	0.0138
7½	2	3½	0.0415	27½	5	5½		47½	8	5½	0.0727	67½	12	5½	0.0208
8	2	4		28	5	5½	0.0166	48	8	6		68	12	5½	0.0276
8½	2	4	0.0415	28½	5	5½	0.0332	48½	9	5	0.0645	68½	12	5½	0.0345
9	2	4½		29	5	5½	0.0498	49	9	5	0.0715	69	12	5½	0.0415
9½	2	4½	0.0415	29½	5	5½	0.0664	49½	9	5½		69½	12	5½	0.0484
10	2	5		30	5	6		50	10	5		70	14	5	
10½	2	5	0.0415	30½	6	5	0.0138	50½	10	5	0.0083	70½	12	5½	0.0622
11	2	5½		31	6	5	0.0276	51	10	5	0.0166	71	12	5½	0.0691
11½	2	5½	0.0415	31½	6	5	0.0414	51½	10	5	0.0249	71½	13	5½	
12	2	6		32	6	5	0.0552	52	9	5½	0.0461	72	12	6	
12½	3	4	0.0276	32½	6	5	0.0691	52½	9	5½	0.0553	72½	13	5½	0.0127
13	3	4	0.0553	33	6	5½		53	9	5½	0.0645	73	13	5½	0.0191
13½	3	4½		33½	6	5½	0.0138	53½	9	5½	0.0737	73½	13	5½	0.0255
14	3	4½	0.0276	34	6	5½	0.0276	54	9	6		74	13	5½	0.0319
14½	3	4½	0.0553	34½	6	5½	0.0415	54½	10	5	0.0747	74½	13	5½	0.0383
15	3	5		35	7	5		55	11	5		75	15	5	
15½	3	5	0.0276	35½	6	5½	0.0691	55½	10	5½	0.0083	75½	13	5½	0.0511
16	3	5	0.0553	36	6	6		56	10	5½	0.0166	76	13	5½	0.0575
16½	3	5½		36½	7	5	0.0355	56½	10	5½	0.0249	76½	13	5½	0.0638
17	3	5½	0.0276	37	7	5	0.0474	57	10	5½	0.0332	77	14	5½	
17½	3	5½	0.0553	37½	7	5	0.0592	57½	10	5½	0.0415	77½	13	5½	0.0766
18	3	6		38	7	5	0.0711	58	10	5½	0.0498	78	13	6	
18½	4	4½	0.0207	38½	7	5½		58½	10	5½	0.0581	78½	14	5½	0.0178
19	4	4½	0.0415	39	7	5½	0.0118	59	10	5½	0.0664	79	14	5½	0.0237
19½	4	4½	0.0622	39½	7	5½	0.0237	59½	10	5½	0.0747	79½	14	5½	0.0296
20	4	5		40	8	5		60	10	6		80	16	5	
20½	4	5	0.0207	40½	7	5½	0.0474	60½	11	5½		80½	14	5½	0.0415
21	4	5	0.0415	41	7	5½	0.0592	61	11	5½	0.0075	81	14	5½	0.0474
21½	4	5	0.0622	41½	7	5½	0.0711	61½	11	5½	0.0151	81½	14	5½	0.0534
22	4	5½		42	7	6		62	11	5½	0.0226	82	14	5½	0.0593
22½	4	5½	0.0207	42½	8	5	0.0519	62½	11	5½	0.0301	82½	15	5½	
23	4	5½	0.0415	43	8	5	0.0622	63	11	5½	0.0377	83	14	5½	0.0711
23½	4	5½	0.0622	43½	8	5	0.0726	63½	11	5½	0.0453	83½	14	5½	0.0771
24	4	6		44	8	5½		64	11	5½	0.0528	84	14	6	
24½	5	4½	0.0664	44½	8	5½	0.0103	64½	11	5½	0.0604	84½	15	5½	0.0221

Pica ems	Adjustments			Pica ems	Adjustments			Pica ems	Adjustments			Pica ems	Adjustments		
	Drum (casts)	Indicator scale (ems)	Micrometer wedge +		Drum (casts)	Indicator scale (ems)	Micrometer wedge +		Drum (casts)	Indicator scale (ems)	Micrometer wedge +		Drum (casts)	Indicator scale (ems)	Micrometer wedge +
85	17	5		100	20	5		115	23	5		130	23	5½	0-0252
85½	15	5½	0-0332	100½	17	5½	0-0683	115½	21	5½		130½	22	5½	0-0716
86	15	5½	0-0387	101	17	5½	0-0732	116	20	5½	0-0498	131	22	5½	0-0754
86½	15	5½	0-0443	101½	17	5½	0-0781	116½	20	5½	0-0540	131½	22	5½	0-0792
87	15	5½	0-0498	102	17	6		117	20	5½	0-0581	132	22	6	
87½	15	5½	0-0553	102½	18	5½	0-0323	117½	20	5½	0-0623	132½	23	5½	0-0433
88	16	5½		103	18	5½	0-0369	118	20	5½	0-0664	133	23	5½	0-0469
88½	15	5½	0-0664	103½	18	5½	0-0415	118½	20	5½	0-0705	133½	23	5½	0-0505
89	15	5½	0-0719	104	18	5½	0-0461	119	20	5½	0-0747	134	23	5½	0-0541
89½	15	5½	0-0774	104½	19	5½		119½	20	5½	0-0788	134½	23	5½	0-0577
90	15	6		105	21	5		120	20	6		135	24	5½	0-0208
90½	16	5½	0-0259	105½	18	5½	0-0599	120½	21	5½	0-0395	135½	23	5½	0-0650
91	16	5½	0-0311	106	18	5½	0-0646	121	22	5½		136	23	5½	0-0686
91½	16	5½	0-0363	106½	18	5½	0-0692	121½	21	5½	0-0474	136½	23	5½	0-0722
92	16	5½	0-0415	107	18	5½	0-0738	122	21	5½	0-0514	137	23	5½	0-0758
92½	16	5½	0-0467	107½	18	5½	0-0784	122½	21	5½	0-0553	137½	25	5½	
93	16	5½	0-0519	108	18	6		123	21	5½	0-0593	138	23	6	
93½	17	5½		108½	19	5½	0-0349	123½	21	5½	0-0632	138½	24	5½	0-0450
94	16	5½	0-0623	109	19	5½	0-0393	124	21	5½	0-0672	139	24	5½	0-0484
94½	16	5½	0-0675	109½	19	5½	0-0437	124½	21	5½	0-0711	139½	24	5½	0-0519
95	19	5		110	22	5		125	25	5		140	25	5½	0-0166
95½	16	5½	0-0778	110½	19	5½	0-0524	125½	21	5½	0-0790	140½	24	5½	0-0583
96	16	6		111	19	5½	0-0568	126	21	6		141	24	5½	0-0623
96½	17	5½	0-0293	111½	19	5½	0-0612	126½	23	5½		141½	24	5½	0-0657
97	17	5½	0-0342	112	19	5½	0-0655	127	22	5½	0-0453	142	24	5½	0-0692
97½	17	5½	0-0391	112½	19	5½	0-0699	127½	22	5½	0-0490	142½	24	5½	0-0726
98	17	5½	0-0439	113	19	5½	0-0743	128	22	5½	0-0528	143	25	5½	0-0365
98½	17	5½	0-0488	113½	19	5½	0-0786	128½	22	5½	0-0566	143½	24	5½	0-0795
99	18	5½		114	19	6		129	22	5½	0-0603	144	24	6	
99½	17	5½	0-0586	114½	20	5½	0-0374	129½	22	5½	0-0641				

The calculations are based upon casting in multiples of 5, 5½ or 6 pica ems per cast, plus any necessary addition in 'thousandths' of an inch. In the section under 'Adjustments' the first column shows the row of the drum which must be brought to 'A' on the remainder scale on the counter mechanism head; the second column shows the position of the pointer on the micrometer indicator scale; and the third shows the addition in 'thousandths' of an inch to be added by the micrometer wedge (this is indicated, as the micrometer wedge is adjusted by the figures on the upper edge of the upper section of the handwheel on the micrometer wedge). The total amount in the third and fourth columns multiplied by the number of casts in the second column, is equivalent to the measure given in the first column.

Cutting strip material (ciceros)

The following table shows the position of the counter drum and the adjustment of the micrometer wedge to shear strip material to ciceros and half-ciceros.

Ciceros	Adjustments			Ciceros	Adjustments			Ciceros	Adjustments			Ciceros	Adjustments		
	Drum (casts)	Indicator scale (ems*)	Micrometer wedge + t		Drum (casts)	Indicator scale (ems*)	Micrometer wedge + t		Drum (casts)	Indicator scale (ems*)	Micrometer wedge + t		Drum (casts)	Indicator scale (ems*)	Micrometer wedge + t
5	1	5	0.0580	21	4	5½	0.0194	37	7	5½	0.0257	53	10	5½	0.0283
5½	1	5½	0.0638	21½	4	5½	0.0416	37½	7	5½	0.0384	53½	10	5½	0.0372
6	2	3	0.0348	22	4	5½	0.0638	38	7	5½	0.0511	54	10	5½	0.0460
6½	2	3	0.0792	22½	5	4½	0.0522	38½	7	5½	0.0638	54½	10	5½	0.0549
7	2	3½	0.0406	23	5	4½	0.0700	39	7	5½	0.0765	55	10	5½	0.0638
7½	2	4	0.0020	23½	5	5	0.0047	39½	8	5	0.0469	55½	10	5½	0.0727
8	2	4	0.0464	24	5	5	0.0225	40	8	5	0.0580	56	10	5½	0.0816
8½	2	4½	0.0078	24½	5	5	0.0402	40½	8	5	0.0691	56½	12	5	0.0062
9	2	4½	0.0522	25	5	5	0.0580	41	8	5	0.0802	57	11	5½	0.0073
9½	2	5	0.0136	25½	5	5	0.0758	41½	8	5½	0.0083	57½	11	5½	0.0154
10	2	5	0.0580	26	5	5½	0.0105	42	8	5½	0.0194	58	11	5½	0.0234
10½	2	5½	0.0194	26½	5	5½	0.0283	42½	8	5½	0.0305	58½	11	5½	0.0315
11	2	5½	0.0638	27	5	5½	0.0460	43	8	5½	0.0416	59	11	5½	0.0396
11½	3	4	0.0168	27½	5	5½	0.0638	43½	8	5½	0.0527	59½	11	5½	0.0477
12	3	4	0.0464	28	5	5½	0.0816	44	8	5½	0.0638	60	11	5½	0.0557
12½	3	4	0.0760	28½	6	5	0.0136	44½	8	5½	0.0749	60½	11	5½	0.0638
13	3	4½	0.0226	29	6	5	0.0284	45	9	5	0.0580	61	11	5½	0.0719
13½	3	4½	0.0522	29½	6	5	0.0432	45½	9	5	0.0679	61½	11	5½	0.0799
14	3	4½	0.0818	30	6	5	0.0580	46	9	5	0.0777	62	12	5½	0.0046
14½	3	5	0.0284	30½	6	5	0.0728	46½	9	5½	0.0046	62½	12	5½	0.0120
15	3	5	0.0580	31	6	5½	0.0046	47	9	5½	0.0145	63	12	5½	0.0194
15½	3	5½	0.0046	31½	6	5½	0.0194	47½	9	5½	0.0243	63½	12	5½	0.0268
16	3	5½	0.0342	32	6	5½	0.0342	48	9	5½	0.0342	64	12	5½	0.0342
16½	3	5½	0.0638	32½	6	5½	0.0490	48½	9	5½	0.0441	64½	12	5½	0.0416
17	4	4½	0.0078	33	6	5½	0.0638	49	9	5½	0.0539	65	12	5½	0.0490
17½	4	4½	0.0300	33½	6	5½	0.0786	49½	9	5½	0.0638	65½	12	5½	0.0564
18	4	4½	0.0522	34	7	5	0.0326	50	9	5½	0.0737	66	12	5½	0.0638
18½	4	4½	0.0744	34½	7	5	0.0453	50½	10	5	0.0669	66½	12	5½	0.0712
19	4	5	0.0136	35	7	5	0.0580	51	10	5	0.0758	67	13	5½	0.0023
19½	4	5	0.0358	35½	7	5	0.0707	51½	10	5½	0.0016	67½	13	5½	0.0092
20	4	5	0.0580	36	7	5½	0.0004	52	10	5½	0.0105	68	13	5½	0.0160
20½	4	5	0.0802	36½	7	5½	0.0131	52½	10	5½	0.0194	68½	13	5½	0.0228

Ciceros	Adjustments			Ciceros	Adjustments			Ciceros	Adjustments			Ciceros	Adjustments		
	Drum (casts)	Indicator scale (ems*)	Micrometer wedge + †		Drum (casts)	Indicator scale (ems*)	Micrometer wedge + †		Drum (casts)	Indicator scale (ems*)	Micrometer wedge + †		Drum (casts)	Indicator scale (ems*)	Micrometer wedge + †
69	13	5½	0.0296	77	14	5½	0.0638	85	16	5½	0.0305	93	18	5½	0.0046
69½	13	5½	0.0365	77½	15	5½	0.0046	85½	16	5½	0.0361	93½	18	5½	0.0095
70	13	5½	0.0433	78	15	5½	0.0105	86	16	5½	0.0416	94	18	5½	0.0145
70½	13	5½	0.0501	78½	15	5½	0.0164	86½	16	5½	0.0472	94½	18	5½	0.0194
71	13	5½	0.0570	79	15	5½	0.0224	87	16	5½	0.0527	95	18	5½	0.0243
71½	13	5½	0.0638	79½	15	5½	0.0283	87½	17	5½	0.0011	95½	18	5½	0.0293
72	14	5½	0.0004	80	15	5½	0.0342	88	17	5½	0.0063	96	18	5½	0.0342
72½	14	5½	0.0067	80½	15	5½	0.0401	88½	17	5½	0.0116	96½	18	5½	0.0391
73	14	5½	0.0131	81	15	5½	0.0460	89	17	5½	0.0168	97	18	5½	0.0441
73½	14	5½	0.0194	81½	15	5½	0.0519	89½	17	5½	0.0220	97½	18	5½	0.0490
74	14	5½	0.0257	82	15	5½	0.0579	90	17	5½	0.0272	98	19	5½	0.0030
74½	14	5½	0.0321	82½	16	5½	0.0028	90½	17	5½	0.0325	98½	19	5½	0.0077
75	14	5½	0.0384	83	16	5½	0.0083	91	17	5½	0.0377	99	19	5½	0.0124
75½	14	5½	0.0448	83½	16	5½	0.0138	91½	17	5½	0.0429	99½	19	5½	0.0171
76	14	5½	0.0511	84	16	5½	0.0194	92	17	5½	0.0481	100	19	5½	0.0217
76½	14	5½	0.0574	84½	16	5½	0.0249	92½	17	5½	0.0534				

*These are pica ems and half ems (0.166 inch). †These figures represent thousandths of an inch.

The calculations are based upon casting in multiples of 5, 5½ or 6 pica ems per cast, plus any necessary addition in 'thousandths' of an inch. In the section under 'Adjustments' the first column shows the row of the drum which must be brought to 'A' on the remainder scale on the counter mechanism head; the second column shows the position of the pointer on the micrometer indicator scale; and the third shows the addition in 'thousandths' of an inch to be added by the micrometer wedge (this is indicated, as the micrometer wedge is adjusted by the figures on the upper edge of the upper section of the handwheel on the micrometer wedge). The total amount in the third and fourth columns multiplied by the number of casts in the second column, is equivalent to the measure given in the first column.

Micrometer head settings

For composition matrices – 5 set to $9\frac{3}{4}$ set – 3 units to 14 units

Upper figures show adjustment in points and fractions of a point of wedge screw handwheel scale;
lower figures show resultant sizes in thousandths of an inch.

Set	Units											
	3	4	5	6	7	8	9	10	11	12	13	14
5	$\frac{27}{32}$ 0.0115	$1\frac{1}{8}$ 0.0154	$1\frac{13}{32}$ 0.0192	$1\frac{1}{4}$ 0.0231	$1\frac{5}{8}$ 0.0269	$2\frac{7}{32}$ 0.0307	$2\frac{1}{2}$ 0.0346	$2\frac{25}{32}$ 0.0384	$3\frac{1}{16}$ 0.0423	$3\frac{11}{32}$ 0.0461	$3\frac{5}{8}$ 0.0500	$3\frac{3}{4}$ 0.0538
$5\frac{1}{4}$	$\frac{7}{8}$ 0.0121	$1\frac{5}{32}$ 0.0161	$1\frac{15}{32}$ 0.0202	$1\frac{3}{4}$ 0.0242	$2\frac{1}{32}$ 0.0282	$2\frac{11}{32}$ 0.0323	$2\frac{5}{8}$ 0.0363	$2\frac{29}{32}$ 0.0403	$3\frac{7}{32}$ 0.0444	$3\frac{1}{2}$ 0.0484	$3\frac{13}{16}$ 0.0525	$4\frac{3}{32}$ 0.0565
$5\frac{1}{2}$	$\frac{29}{32}$ 0.0127	$1\frac{7}{32}$ 0.0169	$1\frac{17}{32}$ 0.0211	$1\frac{27}{32}$ 0.0254	$2\frac{5}{32}$ 0.0296	$2\frac{7}{16}$ 0.0338	$2\frac{3}{4}$ 0.0380	$3\frac{1}{16}$ 0.0423	$3\frac{3}{8}$ 0.0465	$3\frac{21}{32}$ 0.0507	$3\frac{21}{16}$ 0.0549	$4\frac{9}{32}$ 0.0592
$5\frac{3}{4}$	$\frac{31}{32}$ 0.0133	$1\frac{9}{32}$ 0.0177	$1\frac{19}{32}$ 0.0221	$1\frac{29}{32}$ 0.0265	$2\frac{1}{4}$ 0.0309	$2\frac{9}{16}$ 0.0354	$2\frac{7}{8}$ 0.0398	$3\frac{3}{16}$ 0.0442	$3\frac{1}{2}$ 0.0486	$3\frac{27}{32}$ 0.0530	$4\frac{5}{32}$ 0.0574	$4\frac{15}{32}$ 0.0619
6	1 0.0138	$1\frac{11}{32}$ 0.0184	$1\frac{11}{16}$ 0.0231	2 0.0277	$2\frac{11}{32}$ 0.0323	$2\frac{11}{16}$ 0.0369	3 0.0415	$3\frac{11}{32}$ 0.0461	$3\frac{3}{4}$ 0.0507	4 0.0553	$4\frac{11}{32}$ 0.0599	$4\frac{11}{16}$ 0.0646
$6\frac{1}{4}$	$1\frac{1}{32}$ 0.0144	$1\frac{3}{8}$ 0.0192	$1\frac{3}{4}$ 0.0240	$2\frac{3}{32}$ 0.0288	$2\frac{7}{16}$ 0.0336	$2\frac{25}{32}$ 0.0384	$3\frac{1}{8}$ 0.0432	$3\frac{15}{32}$ 0.0480	$3\frac{13}{16}$ 0.0528	$4\frac{5}{32}$ 0.0576	$4\frac{1}{2}$ 0.0624	$4\frac{7}{8}$ 0.0672
$6\frac{1}{2}$	$1\frac{3}{32}$ 0.0150	$1\frac{7}{16}$ 0.0200	$1\frac{13}{16}$ 0.0250	$2\frac{3}{16}$ 0.0300	$2\frac{17}{32}$ 0.0350	$2\frac{29}{32}$ 0.0400	$3\frac{1}{4}$ 0.0450	$3\frac{5}{8}$ 0.0500	$3\frac{31}{32}$ 0.0549	$4\frac{11}{32}$ 0.0599	$4\frac{11}{16}$ 0.0649	$5\frac{1}{16}$ 0.0699
$6\frac{3}{4}$	$1\frac{1}{8}$ 0.0156	$1\frac{1}{2}$ 0.0207	$1\frac{7}{8}$ 0.0259	$2\frac{1}{4}$ 0.0311	$2\frac{5}{8}$ 0.0363	3 0.0415	$3\frac{3}{8}$ 0.0467	$3\frac{3}{4}$ 0.0519	$4\frac{1}{8}$ 0.0571	$4\frac{1}{2}$ 0.0622	$4\frac{7}{8}$ 0.0674	$5\frac{1}{4}$ 0.0726
7	$1\frac{3}{16}$ 0.0161	$1\frac{1}{4}$ 0.0215	$1\frac{11}{16}$ 0.0269	$2\frac{1}{32}$ 0.0323	$2\frac{23}{32}$ 0.0377	$3\frac{1}{8}$ 0.0430	$3\frac{1}{2}$ 0.0484	$3\frac{7}{8}$ 0.0538	$4\frac{9}{32}$ 0.0592	$4\frac{11}{16}$ 0.0646	$5\frac{1}{8}$ 0.0699	$5\frac{7}{16}$ 0.0753
$7\frac{1}{4}$	$1\frac{7}{32}$ 0.0167	$1\frac{5}{8}$ 0.0223	$2\frac{1}{32}$ 0.0279	$2\frac{13}{32}$ 0.0334	$2\frac{13}{16}$ 0.0390	$3\frac{7}{32}$ 0.0446	$3\frac{5}{8}$ 0.0501	$4\frac{1}{32}$ 0.0557	$4\frac{7}{16}$ 0.0613	$4\frac{27}{32}$ 0.0669	$5\frac{1}{4}$ 0.0724	$5\frac{21}{32}$ 0.0780
$7\frac{1}{2}$	$1\frac{1}{4}$ 0.0173	$1\frac{11}{16}$ 0.0231	$2\frac{3}{32}$ 0.0288	$2\frac{1}{2}$ 0.0346	$2\frac{29}{32}$ 0.0403	$3\frac{11}{32}$ 0.0461	$3\frac{3}{4}$ 0.0519	$4\frac{5}{32}$ 0.0576	$4\frac{19}{32}$ 0.0634	5 0.0692	$5\frac{13}{32}$ 0.0749	$5\frac{27}{32}$ 0.0807
$7\frac{3}{4}$	$1\frac{9}{32}$ 0.0179	$1\frac{23}{32}$ 0.0238	$2\frac{5}{32}$ 0.0298	$2\frac{9}{32}$ 0.0357	3 0.0417	$3\frac{7}{16}$ 0.0476	$3\frac{7}{8}$ 0.0536	$4\frac{5}{16}$ 0.0596	$4\frac{3}{4}$ 0.0655	$5\frac{3}{16}$ 0.0715	$5\frac{19}{32}$ 0.0774	$6\frac{1}{32}$ 0.0834
8	$1\frac{11}{32}$ 0.0184	$1\frac{25}{32}$ 0.0246	$2\frac{7}{32}$ 0.0307	$2\frac{11}{16}$ 0.0369	$3\frac{1}{8}$ 0.0430	$3\frac{9}{16}$ 0.0492	4 0.0553	$4\frac{7}{16}$ 0.0615	$4\frac{7}{8}$ 0.0676	$5\frac{11}{32}$ 0.0738	$5\frac{25}{32}$ 0.0799	$6\frac{7}{32}$ 0.0861
$8\frac{1}{4}$	$1\frac{3}{8}$ 0.0190	$1\frac{27}{32}$ 0.0254	$2\frac{5}{16}$ 0.0317	$2\frac{3}{4}$ 0.0380	$3\frac{7}{32}$ 0.0444	$3\frac{21}{32}$ 0.0507	$4\frac{1}{8}$ 0.0571	$4\frac{19}{32}$ 0.0634	$5\frac{3}{32}$ 0.0697	$5\frac{1}{2}$ 0.0761	$5\frac{31}{32}$ 0.0824	$6\frac{13}{32}$ 0.0888
$8\frac{1}{2}$	$1\frac{13}{32}$ 0.0196	$1\frac{7}{8}$ 0.0261	$2\frac{3}{8}$ 0.0327	$2\frac{27}{32}$ 0.0392	$3\frac{5}{16}$ 0.0457	$3\frac{25}{32}$ 0.0523	$4\frac{1}{4}$ 0.0588	$4\frac{23}{32}$ 0.0653	$5\frac{3}{16}$ 0.0719	$5\frac{11}{16}$ 0.0784	$6\frac{1}{8}$ 0.0849	$6\frac{5}{8}$ 0.0915
$8\frac{3}{4}$	$1\frac{15}{32}$ 0.0202	$1\frac{15}{16}$ 0.0269	$2\frac{7}{16}$ 0.0336	$2\frac{29}{32}$ 0.0403	$3\frac{13}{32}$ 0.0471	$3\frac{7}{8}$ 0.0538	$4\frac{3}{8}$ 0.0605	$4\frac{7}{8}$ 0.0672	$5\frac{11}{32}$ 0.0740	$5\frac{27}{32}$ 0.0807	$6\frac{5}{16}$ 0.0874	$6\frac{13}{16}$ 0.0941
9	$1\frac{1}{2}$ 0.0207	2 0.0277	$2\frac{1}{2}$ 0.0346	3 0.0415	$3\frac{1}{2}$ 0.0484	4 0.0553	$4\frac{1}{2}$ 0.0622	5 0.0692	$5\frac{1}{2}$ 0.0761	6 0.0830	$6\frac{1}{2}$ 0.0899	7 0.0968
$9\frac{1}{4}$	$1\frac{17}{32}$ 0.0213	$2\frac{1}{16}$ 0.0284	$2\frac{9}{16}$ 0.0355	$3\frac{3}{32}$ 0.0427	$3\frac{19}{32}$ 0.0498	$4\frac{1}{8}$ 0.0569	$4\frac{5}{8}$ 0.0640	$5\frac{5}{32}$ 0.0711	$5\frac{21}{32}$ 0.0782	$6\frac{5}{32}$ 0.0853	$6\frac{11}{16}$ 0.0924	$7\frac{1}{16}$ 0.0995
$9\frac{1}{2}$	$1\frac{19}{32}$ 0.0219	$2\frac{1}{8}$ 0.0292	$2\frac{21}{32}$ 0.0365	$3\frac{5}{32}$ 0.0438	$3\frac{11}{16}$ 0.0511	$4\frac{7}{32}$ 0.0584	$4\frac{3}{4}$ 0.0657	$5\frac{9}{32}$ 0.0730	$5\frac{17}{16}$ 0.0803	$6\frac{11}{32}$ 0.0876	$6\frac{7}{8}$ 0.0949	$7\frac{13}{32}$ 0.1022
$9\frac{3}{4}$	$1\frac{5}{8}$ 0.0225	$2\frac{3}{16}$ 0.0300	$2\frac{29}{32}$ 0.0375	3 0.0450	$3\frac{1}{4}$ 0.0525	$4\frac{11}{32}$ 0.0599	$4\frac{7}{8}$ 0.0674	$5\frac{13}{16}$ 0.0749	$5\frac{31}{32}$ 0.0824	$6\frac{1}{2}$ 0.0899	$7\frac{1}{32}$ 0.0974	$7\frac{9}{32}$ 0.1049

For composition matrices – 5 set to $9\frac{3}{4}$ set – 15 units to 26 units

Set	Units											
	15	16	17	18	19	20	21	22	23	24	25	26
5	$4\frac{5}{32}$ 0.0576	$4\frac{7}{16}$ 0.0615	$4\frac{23}{32}$ 0.0653	5 0.0692	$5\frac{9}{32}$ 0.0730	$5\frac{9}{16}$ 0.0769	$5\frac{27}{32}$ 0.0807	$6\frac{1}{8}$ 0.0845	$6\frac{3}{8}$ 0.0884	$6\frac{21}{32}$ 0.0922	$6\frac{15}{16}$ 0.0961	$7\frac{7}{32}$ 0.0999
$5\frac{1}{4}$	$4\frac{3}{8}$ 0.0605	$4\frac{11}{16}$ 0.0646	$4\frac{31}{32}$ 0.0686	$5\frac{1}{4}$ 0.0726	$5\frac{5}{16}$ 0.0767	$5\frac{27}{32}$ 0.0807	$6\frac{1}{8}$ 0.0847	$6\frac{13}{32}$ 0.0888	$6\frac{23}{32}$ 0.0928	7 0.0968	$7\frac{9}{32}$ 0.1009	$7\frac{19}{32}$ 0.1049
$5\frac{1}{2}$	$4\frac{19}{32}$ 0.0634	$4\frac{7}{8}$ 0.0676	$5\frac{3}{16}$ 0.0719	$5\frac{1}{2}$ 0.0761	$5\frac{13}{16}$ 0.0803	$6\frac{1}{8}$ 0.0845	$6\frac{13}{32}$ 0.0888	$6\frac{23}{32}$ 0.0930	$7\frac{1}{32}$ 0.0972	$7\frac{11}{32}$ 0.1014	$7\frac{21}{32}$ 0.1057	$7\frac{15}{16}$ 0.1099
$5\frac{3}{4}$	$4\frac{13}{16}$ 0.0663	$5\frac{1}{8}$ 0.0707	$5\frac{7}{16}$ 0.0751	$5\frac{3}{4}$ 0.0795	$6\frac{1}{16}$ 0.0840	$6\frac{13}{32}$ 0.0884	$6\frac{23}{32}$ 0.0928	$7\frac{1}{32}$ 0.0972	$7\frac{11}{32}$ 0.1016	$7\frac{21}{32}$ 0.1060	8 0.1105	$8\frac{5}{16}$ 0.1149
6	5 0.0692	$5\frac{11}{32}$ 0.0738	$5\frac{11}{16}$ 0.0784	6 0.0830	$6\frac{11}{32}$ 0.0876	$6\frac{21}{32}$ 0.0922	7 0.0968	$7\frac{1}{32}$ 0.1014	$7\frac{21}{32}$ 0.1061	8 0.1106	$8\frac{11}{16}$ 0.1153	$8\frac{11}{16}$ 0.1199
$6\frac{1}{4}$	$5\frac{7}{32}$ 0.0720	$5\frac{9}{16}$ 0.0769	$5\frac{23}{32}$ 0.0817	$6\frac{1}{4}$ 0.0865	$6\frac{19}{32}$ 0.0913	$6\frac{15}{16}$ 0.0961	$7\frac{5}{16}$ 0.1009	$7\frac{31}{32}$ 0.1057	8 0.1105	$8\frac{11}{32}$ 0.1152	$8\frac{11}{16}$ 0.1201	$9\frac{1}{32}$ 0.1249
$6\frac{1}{2}$	$5\frac{13}{32}$ 0.0749	$5\frac{25}{32}$ 0.0799	$6\frac{1}{8}$ 0.0849	$6\frac{1}{2}$ 0.0899	$6\frac{7}{8}$ 0.0949	$7\frac{7}{32}$ 0.0999	$7\frac{19}{32}$ 0.1049	$7\frac{15}{16}$ 0.1099	$8\frac{5}{16}$ 0.1149	$8\frac{21}{32}$ 0.1198	$9\frac{1}{32}$ 0.1249	$9\frac{9}{16}$ 0.1299
$6\frac{3}{4}$	$5\frac{5}{8}$ 0.0778	6 0.0830	$6\frac{3}{8}$ 0.0882	$6\frac{3}{4}$ 0.0934	$7\frac{1}{8}$ 0.0986	$7\frac{1}{2}$ 0.1037	$7\frac{7}{8}$ 0.1089	$8\frac{1}{4}$ 0.1141	$8\frac{5}{8}$ 0.1193	9 0.1244	$9\frac{3}{8}$ 0.1297	$9\frac{3}{4}$ 0.1349
7	$5\frac{27}{32}$ 0.0807	$6\frac{7}{32}$ 0.0861	$6\frac{5}{8}$ 0.0915	7 0.0968	$7\frac{13}{32}$ 0.1022	$7\frac{25}{32}$ 0.1076	$8\frac{5}{32}$ 0.1130	$8\frac{9}{16}$ 0.1184	$8\frac{15}{16}$ 0.1237	$9\frac{11}{32}$ 0.1291	$9\frac{23}{32}$ 0.1345	$10\frac{1}{8}$ 0.1399
$7\frac{1}{4}$	$6\frac{1}{32}$ 0.0836	$6\frac{7}{16}$ 0.0892	$6\frac{23}{32}$ 0.0947	$7\frac{1}{4}$ 0.1003	$7\frac{9}{32}$ 0.1059	$8\frac{1}{16}$ 0.1114	$8\frac{15}{32}$ 0.1170	$8\frac{7}{8}$ 0.1226	$9\frac{1}{4}$ 0.1281	$9\frac{21}{32}$ 0.1337	$10\frac{1}{16}$ 0.1393	$10\frac{15}{16}$ 0.1449
$7\frac{1}{2}$	$6\frac{1}{4}$ 0.0865	$6\frac{21}{32}$ 0.0922	$7\frac{3}{32}$ 0.0980	$7\frac{1}{2}$ 0.1038	$7\frac{29}{32}$ 0.1095	$8\frac{11}{32}$ 0.1153	$8\frac{3}{4}$ 0.1210	$9\frac{5}{32}$ 0.1268	$9\frac{19}{32}$ 0.1325	10 0.1383	$10\frac{13}{32}$ 0.1441	$10\frac{27}{32}$ 0.1499
$7\frac{3}{4}$	$6\frac{15}{32}$ 0.0893	$6\frac{7}{8}$ 0.0953	$7\frac{5}{16}$ 0.1013	$7\frac{3}{4}$ 0.1072	$8\frac{3}{16}$ 0.1132	$8\frac{5}{8}$ 0.1191	$9\frac{1}{32}$ 0.1251	$9\frac{15}{32}$ 0.1310	$9\frac{29}{32}$ 0.1369	$10\frac{11}{32}$ 0.1429	$10\frac{21}{16}$ 0.1489	$11\frac{3}{16}$ 0.1549
8	$6\frac{21}{32}$ 0.0922	$7\frac{1}{8}$ 0.0984	$7\frac{9}{16}$ 0.1045	8 0.1107	$8\frac{7}{16}$ 0.1168	$8\frac{7}{8}$ 0.1230	$9\frac{11}{32}$ 0.1291	$9\frac{25}{32}$ 0.1353	$10\frac{7}{32}$ 0.1414	$10\frac{21}{32}$ 0.1475	$11\frac{1}{8}$ 0.1537	$11\frac{9}{16}$ 0.1599
$8\frac{1}{4}$	$6\frac{7}{8}$ 0.0951	$7\frac{13}{32}$ 0.1014	$7\frac{13}{16}$ 0.1078	$8\frac{1}{4}$ 0.1141	$8\frac{23}{32}$ 0.1205	$9\frac{5}{32}$ 0.1268	$9\frac{5}{8}$ 0.1331	$10\frac{3}{32}$ 0.1395	$10\frac{17}{32}$ 0.1458	11 0.1521	$11\frac{15}{16}$ 0.1585	$11\frac{29}{32}$ 0.1648
$8\frac{1}{2}$	$7\frac{3}{32}$ 0.0980	$7\frac{9}{16}$ 0.1045	$8\frac{1}{32}$ 0.1111	$8\frac{1}{2}$ 0.1176	$8\frac{31}{32}$ 0.1241	$9\frac{7}{16}$ 0.1307	$9\frac{29}{32}$ 0.1372	$10\frac{13}{32}$ 0.1437	$10\frac{27}{8}$ 0.1502	$11\frac{11}{32}$ 0.1567	$11\frac{19}{16}$ 0.1633	$12\frac{9}{32}$ 0.1698
$8\frac{3}{4}$	$7\frac{5}{16}$ 0.1009	$7\frac{25}{32}$ 0.1076	$8\frac{1}{4}$ 0.1143	$8\frac{3}{4}$ 0.1210	$9\frac{1}{4}$ 0.1278	$9\frac{23}{32}$ 0.1345	$10\frac{7}{32}$ 0.1412	$10\frac{11}{16}$ 0.1479	$11\frac{3}{16}$ 0.1546	$11\frac{23}{32}$ 0.1613	$12\frac{5}{32}$ 0.1681	$12\frac{15}{16}$ 0.1748
9	$7\frac{1}{2}$ 0.1037	8 0.1107	$8\frac{1}{2}$ 0.1176	9 0.1245	$9\frac{1}{2}$ 0.1314	10 0.1383	$10\frac{1}{2}$ 0.1452	11 0.1522	$11\frac{1}{2}$ 0.1591	12 0.1660	$12\frac{1}{2}$ 0.1729	13 0.1798
$9\frac{1}{4}$	$7\frac{23}{32}$ 0.1066	$8\frac{7}{32}$ 0.1137	$8\frac{3}{4}$ 0.1208	$9\frac{1}{4}$ 0.1280	$9\frac{25}{32}$ 0.1351	$10\frac{9}{32}$ 0.1422	$10\frac{19}{32}$ 0.1493	$11\frac{5}{16}$ 0.1564	$11\frac{19}{32}$ 0.1635	$12\frac{11}{32}$ 0.1706	$12\frac{27}{32}$ 0.1777	$13\frac{3}{8}$ 0.1848
$9\frac{1}{2}$	$7\frac{29}{32}$ 0.1095	$8\frac{7}{16}$ 0.1168	$8\frac{31}{32}$ 0.1241	$9\frac{1}{2}$ 0.1314	$10\frac{1}{32}$ 0.1387	$10\frac{9}{16}$ 0.1460	$11\frac{3}{32}$ 0.1533	$11\frac{5}{8}$ 0.1606	$12\frac{1}{8}$ 0.1679	$12\frac{21}{32}$ 0.1752	$13\frac{3}{16}$ 0.1825	$13\frac{23}{32}$ 0.1898
$9\frac{3}{4}$	$8\frac{1}{8}$ 0.1124	$8\frac{21}{32}$ 0.1199	$9\frac{7}{32}$ 0.1274	$9\frac{3}{4}$ 0.1349	$10\frac{5}{16}$ 0.1424	$10\frac{27}{32}$ 0.1499	$11\frac{3}{8}$ 0.1574	$11\frac{29}{32}$ 0.1648	$12\frac{15}{32}$ 0.1723	13 0.1798	$13\frac{17}{32}$ 0.1873	$14\frac{3}{32}$ 0.1948

Micrometer head settings (continued)

For composition matrices – 10 set to 14 set – 3 units to 14 units

Upper figures show adjustment in points and fractions of a point of wedge screw handwheel scale; lower figures show resultant sizes in thousandths of an inch.

Set	Units											
	3	4	5	6	7	8	9	10	11	12	13	14
10	$1\frac{1}{8}$ 0.0231	$2\frac{7}{32}$ 0.0307	$2\frac{25}{32}$ 0.0384	$3\frac{11}{32}$ 0.0461	$3\frac{7}{8}$ 0.0538	$4\frac{7}{16}$ 0.0615	5 0.0692	$5\frac{9}{16}$ 0.0769	$6\frac{1}{8}$ 0.0845	$6\frac{21}{32}$ 0.0922	$7\frac{7}{32}$ 0.0999	$7\frac{27}{32}$ 0.1076
10 $\frac{1}{4}$	$1\frac{23}{32}$ 0.0236	$2\frac{9}{32}$ 0.0315	$2\frac{27}{32}$ 0.0394	$3\frac{13}{32}$ 0.0473	4 0.0551	$4\frac{9}{16}$ 0.0630	$5\frac{1}{8}$ 0.0709	$5\frac{23}{32}$ 0.0788	$6\frac{9}{32}$ 0.0867	$6\frac{27}{32}$ 0.0945	$7\frac{13}{32}$ 0.1024	$7\frac{31}{32}$ 0.1103
10 $\frac{1}{2}$	$1\frac{3}{4}$ 0.0242	$2\frac{11}{32}$ 0.0323	$2\frac{29}{32}$ 0.0403	$3\frac{1}{2}$ 0.0484	$4\frac{3}{32}$ 0.0565	$4\frac{11}{16}$ 0.0646	$5\frac{1}{4}$ 0.0726	$5\frac{27}{32}$ 0.0807	$6\frac{3}{32}$ 0.0888	7 0.0968	$7\frac{19}{32}$ 0.1049	$8\frac{5}{32}$ 0.1130
10 $\frac{3}{4}$	$1\frac{7}{8}$ 0.0248	$2\frac{13}{32}$ 0.0330	3 0.0413	$3\frac{13}{32}$ 0.0496	$4\frac{1}{16}$ 0.0578	$4\frac{25}{32}$ 0.0661	$5\frac{3}{8}$ 0.0744	$5\frac{31}{32}$ 0.0826	$6\frac{9}{16}$ 0.0909	$7\frac{5}{32}$ 0.0991	$7\frac{25}{32}$ 0.1074	$8\frac{3}{8}$ 0.1157
11	$1\frac{27}{32}$ 0.0254	$2\frac{7}{16}$ 0.0338	$3\frac{1}{16}$ 0.0423	$3\frac{21}{32}$ 0.0507	$4\frac{9}{32}$ 0.0592	$4\frac{7}{8}$ 0.0676	$5\frac{1}{2}$ 0.0761	$6\frac{1}{8}$ 0.0845	$6\frac{23}{32}$ 0.0930	$7\frac{11}{32}$ 0.1014	$7\frac{15}{16}$ 0.1099	$8\frac{7}{16}$ 0.1184
11 $\frac{1}{4}$	$1\frac{7}{8}$ 0.0259	$2\frac{1}{2}$ 0.0346	$3\frac{1}{8}$ 0.0432	$3\frac{3}{4}$ 0.0519	$4\frac{3}{8}$ 0.0605	5 0.0692	$5\frac{5}{8}$ 0.0778	$6\frac{1}{4}$ 0.0865	$6\frac{7}{8}$ 0.0951	$7\frac{1}{2}$ 0.1037	$8\frac{1}{8}$ 0.1124	$8\frac{3}{4}$ 0.1210
11 $\frac{1}{2}$	$1\frac{29}{32}$ 0.0265	$2\frac{9}{16}$ 0.0354	$3\frac{3}{16}$ 0.0442	$3\frac{27}{32}$ 0.0530	$4\frac{15}{32}$ 0.0619	$5\frac{1}{8}$ 0.0707	$5\frac{3}{4}$ 0.0795	$6\frac{13}{32}$ 0.0884	$7\frac{1}{32}$ 0.0972	$7\frac{1}{8}$ 0.1061	$8\frac{5}{16}$ 0.1149	$8\frac{15}{16}$ 0.1237
11 $\frac{3}{4}$	$1\frac{31}{32}$ 0.0271	$2\frac{5}{8}$ 0.0361	$3\frac{1}{4}$ 0.0452	$3\frac{29}{32}$ 0.0542	$4\frac{9}{16}$ 0.0632	$5\frac{3}{32}$ 0.0722	$5\frac{7}{8}$ 0.0813	$6\frac{17}{32}$ 0.0903	$7\frac{3}{16}$ 0.0993	$7\frac{27}{32}$ 0.1084	$8\frac{1}{2}$ 0.1174	$9\frac{1}{8}$ 0.1264
12	2 0.0277	$2\frac{1}{8}$ 0.0369	$3\frac{1}{32}$ 0.0461	4 0.0553	$4\frac{1}{8}$ 0.0646	$5\frac{1}{32}$ 0.0738	6 0.0830	$6\frac{21}{32}$ 0.0922	$7\frac{11}{32}$ 0.1014	8 0.1107	$8\frac{21}{32}$ 0.1199	$9\frac{11}{32}$ 0.1291
12 $\frac{1}{4}$	$2\frac{1}{32}$ 0.0282	$2\frac{23}{32}$ 0.0377	$3\frac{13}{32}$ 0.0471	$4\frac{3}{32}$ 0.0565	$4\frac{25}{32}$ 0.0659	$5\frac{7}{16}$ 0.0753	$6\frac{1}{8}$ 0.0847	$6\frac{13}{16}$ 0.0941	$7\frac{1}{32}$ 0.1036	$8\frac{5}{32}$ 0.1130	$8\frac{27}{32}$ 0.1224	$9\frac{17}{32}$ 0.1318
12 $\frac{1}{2}$	$2\frac{3}{32}$ 0.0288	$2\frac{25}{32}$ 0.0384	$3\frac{15}{32}$ 0.0480	$4\frac{5}{32}$ 0.0576	$4\frac{7}{8}$ 0.0672	$5\frac{9}{16}$ 0.0769	$6\frac{1}{4}$ 0.0865	$6\frac{15}{16}$ 0.0961	$7\frac{21}{32}$ 0.1057	$8\frac{11}{32}$ 0.1153	$9\frac{1}{32}$ 0.1249	$9\frac{23}{32}$ 0.1345
12 $\frac{3}{4}$	$2\frac{5}{16}$ 0.0294	$2\frac{27}{32}$ 0.0392	$3\frac{17}{32}$ 0.0490	$4\frac{1}{4}$ 0.0587	$4\frac{31}{32}$ 0.0685	$5\frac{21}{32}$ 0.0784	$6\frac{3}{8}$ 0.0882	$7\frac{3}{32}$ 0.0980	$7\frac{25}{32}$ 0.1078	$8\frac{1}{2}$ 0.1176	$9\frac{3}{32}$ 0.1274	$9\frac{29}{32}$ 0.1372
13	$2\frac{5}{32}$ 0.0300	$2\frac{7}{8}$ 0.0400	$3\frac{5}{8}$ 0.0500	$4\frac{11}{32}$ 0.0599	$5\frac{1}{16}$ 0.0699	$5\frac{25}{32}$ 0.0799	$6\frac{1}{2}$ 0.0899	$7\frac{7}{32}$ 0.0999	$7\frac{15}{16}$ 0.1099	$8\frac{21}{32}$ 0.1199	$9\frac{3}{8}$ 0.1299	$10\frac{1}{8}$ 0.1399
13 $\frac{1}{4}$	$2\frac{7}{32}$ 0.0305	$2\frac{15}{16}$ 0.0407	$3\frac{11}{16}$ 0.0509	$4\frac{13}{32}$ 0.0610	$5\frac{5}{32}$ 0.0712	$5\frac{7}{8}$ 0.0815	$6\frac{5}{8}$ 0.0916	$7\frac{3}{8}$ 0.1018	$8\frac{3}{32}$ 0.1120	$8\frac{27}{32}$ 0.1222	$9\frac{9}{16}$ 0.1324	$10\frac{5}{16}$ 0.1426
13 $\frac{1}{2}$	$2\frac{1}{4}$ 0.0311	3 0.0415	$3\frac{3}{4}$ 0.0519	$4\frac{1}{2}$ 0.0622	$5\frac{1}{4}$ 0.0726	6 0.0830	$6\frac{3}{4}$ 0.0934	$7\frac{1}{2}$ 0.1037	8 $\frac{1}{4}$ 0.1141	9 0.1245	$9\frac{3}{4}$ 0.1349	$10\frac{1}{2}$ 0.1453
13 $\frac{3}{4}$	$2\frac{9}{32}$ 0.0317	$3\frac{1}{16}$ 0.0423	$3\frac{13}{16}$ 0.0528	$4\frac{19}{32}$ 0.0633	$5\frac{11}{32}$ 0.0739	$6\frac{3}{32}$ 0.0845	$6\frac{7}{8}$ 0.0951	$7\frac{21}{32}$ 0.1057	$8\frac{13}{32}$ 0.1162	$9\frac{5}{32}$ 0.1268	$9\frac{15}{16}$ 0.1374	$10\frac{11}{16}$ 0.1479
14	$2\frac{11}{32}$ 0.0323	$3\frac{3}{32}$ 0.0430	$3\frac{7}{8}$ 0.0538	$4\frac{21}{32}$ 0.0645	$5\frac{7}{16}$ 0.0753	$6\frac{3}{32}$ 0.0861	7 0.0968	$7\frac{25}{32}$ 0.1076	$8\frac{9}{16}$ 0.1184	$9\frac{11}{32}$ 0.1291	$10\frac{1}{8}$ 0.1399	$10\frac{7}{8}$ 0.1506

For composition matrices – 10 set to 14 set – 15 units to 26 units

Set	Units											
	15	16	17	18	19	20	21	22	23	24	25	26
10	$8\frac{11}{32}$ 0.1153	$8\frac{7}{8}$ 0.1230	$9\frac{7}{16}$ 0.1306	10	$10\frac{9}{16}$ 0.1460	$11\frac{1}{8}$ 0.1537	$11\frac{21}{32}$ 0.1614	$12\frac{7}{32}$ 0.1691	$12\frac{25}{32}$ 0.1767	$13\frac{11}{32}$ 0.1844	$13\frac{7}{8}$ 0.1921	$14\frac{7}{16}$ 0.1998
10 $\frac{1}{4}$	$8\frac{17}{32}$ 0.1182	$9\frac{1}{8}$ 0.1260	$9\frac{11}{16}$ 0.1339	10$\frac{1}{4}$	$10\frac{13}{16}$ 0.1497	$11\frac{13}{32}$ 0.1576	$11\frac{31}{32}$ 0.1654	$12\frac{17}{32}$ 0.1733	$13\frac{3}{32}$ 0.1811	$13\frac{21}{32}$ 0.1890	$14\frac{1}{4}$ 0.1969	$14\frac{13}{16}$ 0.2048
10 $\frac{1}{2}$	$8\frac{3}{4}$ 0.1210	$9\frac{11}{32}$ 0.1291	$9\frac{23}{32}$ 0.1372	10$\frac{1}{2}$	$11\frac{3}{32}$ 0.1533	$11\frac{21}{32}$ 0.1614	$12\frac{1}{4}$ 0.1695	$12\frac{27}{32}$ 0.1775	$13\frac{13}{32}$ 0.1855	14 0.1936	$14\frac{19}{32}$ 0.2017	$15\frac{5}{32}$ 0.2098
10 $\frac{3}{4}$	$8\frac{31}{32}$ 0.1239	$9\frac{1}{8}$ 0.1322	$10\frac{5}{32}$ 0.1404	10$\frac{3}{4}$	$11\frac{11}{32}$ 0.1570	$11\frac{15}{16}$ 0.1652	$12\frac{17}{32}$ 0.1735	$13\frac{5}{32}$ 0.1818	$13\frac{3}{4}$ 0.1899	$14\frac{11}{32}$ 0.1982	$14\frac{15}{16}$ 0.2065	$15\frac{13}{32}$ 0.2148
11	$9\frac{5}{32}$ 0.1268	$9\frac{25}{32}$ 0.1353	$10\frac{13}{32}$ 0.1437	11	$11\frac{5}{8}$ 0.1606	$12\frac{7}{32}$ 0.1691	$12\frac{27}{32}$ 0.1775	$13\frac{7}{16}$ 0.1860	$14\frac{1}{8}$ 0.1944	$14\frac{21}{32}$ 0.2029	$15\frac{9}{32}$ 0.2113	$15\frac{7}{8}$ 0.2198
11 $\frac{1}{4}$	$9\frac{3}{8}$ 0.1297	10 0.1383	$10\frac{5}{8}$ 0.1470	11$\frac{1}{4}$	$11\frac{7}{8}$ 0.1643	$12\frac{1}{2}$ 0.1729	$13\frac{1}{8}$ 0.1816	$13\frac{3}{4}$ 0.1902	$14\frac{3}{8}$ 0.1988	15 0.2075	$15\frac{5}{8}$ 0.2161	$16\frac{1}{4}$ 0.2248
11 $\frac{1}{2}$	$9\frac{19}{32}$ 0.1326	$10\frac{7}{32}$ 0.1414	$10\frac{7}{8}$ 0.1502	11$\frac{1}{2}$	$12\frac{1}{8}$ 0.1679	$12\frac{25}{32}$ 0.1768	$13\frac{13}{32}$ 0.1856	$14\frac{1}{16}$ 0.1944	$14\frac{11}{16}$ 0.2032	$15\frac{11}{32}$ 0.2121	$15\frac{31}{32}$ 0.2209	$16\frac{5}{8}$ 0.2298
11 $\frac{3}{4}$	$9\frac{13}{16}$ 0.1355	$10\frac{7}{16}$ 0.1445	$11\frac{3}{32}$ 0.1535	11$\frac{3}{4}$	$12\frac{13}{32}$ 0.1716	$13\frac{1}{16}$ 0.1806	$13\frac{29}{32}$ 0.1896	$14\frac{3}{8}$ 0.1987	$15\frac{1}{32}$ 0.2076	$15\frac{21}{32}$ 0.2167	$16\frac{5}{16}$ 0.2257	$16\frac{31}{32}$ 0.2348
12	10 0.1383	$10\frac{11}{16}$ 0.1476	$11\frac{11}{32}$ 0.1568	12	$12\frac{21}{32}$ 0.1752	$13\frac{11}{32}$ 0.1844	14 0.1937	$14\frac{11}{16}$ 0.2029	$15\frac{11}{32}$ 0.2121	16 0.2213	$16\frac{11}{16}$ 0.2306	$17\frac{11}{32}$ 0.2398
12 $\frac{1}{4}$	$10\frac{7}{32}$ 0.1412	$10\frac{7}{8}$ 0.1506	$11\frac{9}{16}$ 0.1600	12$\frac{1}{4}$	$12\frac{15}{16}$ 0.1789	$13\frac{5}{8}$ 0.1883	$14\frac{5}{16}$ 0.1977	$14\frac{31}{32}$ 0.2071	$15\frac{21}{32}$ 0.2165	$16\frac{11}{32}$ 0.2259	17 0.2354	$17\frac{11}{16}$ 0.2448
12 $\frac{1}{2}$	$10\frac{13}{32}$ 0.1441	$11\frac{1}{8}$ 0.1537	$11\frac{13}{16}$ 0.1633	12$\frac{1}{2}$	$13\frac{3}{16}$ 0.1825	$13\frac{7}{8}$ 0.1921	$14\frac{13}{32}$ 0.2017	$15\frac{9}{32}$ 0.2113	$15\frac{31}{32}$ 0.2209	$16\frac{11}{16}$ 0.2305	$17\frac{3}{8}$ 0.2402	$18\frac{1}{16}$ 0.2498
12 $\frac{3}{4}$	$10\frac{5}{8}$ 0.1470	$11\frac{11}{32}$ 0.1568	$12\frac{1}{32}$ 0.1666	12$\frac{3}{4}$	$13\frac{15}{32}$ 0.1862	$14\frac{5}{32}$ 0.1960	$14\frac{7}{8}$ 0.2058	$15\frac{13}{32}$ 0.2156	$16\frac{9}{32}$ 0.2253	17 0.2351	$17\frac{23}{32}$ 0.2450	$18\frac{13}{32}$ 0.2548
13	$10\frac{27}{32}$ 0.1499	$11\frac{9}{16}$ 0.1599	$12\frac{9}{32}$ 0.1698	13	$13\frac{23}{32}$ 0.1898	$14\frac{7}{16}$ 0.1998	$15\frac{5}{32}$ 0.2098	$15\frac{7}{8}$ 0.2198	$16\frac{5}{8}$ 0.2298	$17\frac{11}{32}$ 0.2398	$18\frac{1}{16}$ 0.2498	$18\frac{25}{32}$ 0.2598
13 $\frac{1}{4}$	$11\frac{1}{32}$ 0.1528	$11\frac{25}{32}$ 0.1629	$12\frac{1}{2}$ 0.1731	13$\frac{1}{4}$	14 0.1935	$14\frac{23}{32}$ 0.2037	$15\frac{13}{32}$ 0.2138	$16\frac{3}{16}$ 0.2240	$16\frac{15}{16}$ 0.2342	$17\frac{21}{32}$ 0.2444	$18\frac{13}{32}$ 0.2546	$19\frac{1}{8}$ 0.2647
13 $\frac{1}{2}$	$11\frac{1}{4}$ 0.1556	12 0.1660	$12\frac{3}{4}$ 0.1764	13$\frac{1}{2}$	$14\frac{1}{4}$ 0.1971	15 0.2075	$15\frac{3}{4}$ 0.2179	$16\frac{1}{2}$ 0.2282	$17\frac{1}{4}$ 0.2386	18 0.2490	$18\frac{3}{4}$ 0.2594	$19\frac{1}{2}$ 0.2697
13 $\frac{3}{4}$	$11\frac{15}{32}$ 0.1585	$12\frac{7}{32}$ 0.1691	13 0.1796	13$\frac{3}{4}$	$14\frac{1}{2}$ 0.2008	$15\frac{9}{32}$ 0.2113	$16\frac{1}{32}$ 0.2219	$16\frac{13}{16}$ 0.2325	$17\frac{9}{16}$ 0.2430	$18\frac{11}{32}$ 0.2536	$19\frac{3}{32}$ 0.2642	19 0.2747
14	$11\frac{21}{32}$ 0.1614	$12\frac{7}{16}$ 0.1722	$13\frac{7}{32}$ 0.1829	14	$14\frac{25}{32}$ 0.2044	$15\frac{9}{16}$ 0.2152	$16\frac{11}{32}$ 0.2259	$17\frac{1}{4}$ 0.2367	$17\frac{7}{8}$ 0.2474	$18\frac{21}{32}$ 0.2582	$19\frac{7}{16}$ 0.2690	$20\frac{7}{32}$ 0.2797

Micrometer head settings (continued)

For large composition matrices – 14 set to $18\frac{3}{4}$ set –3 units to 14 units

Upper figures show adjustment in points and fractions of a point of wedge screw handwheel scale;
lower figures show resultant sizes in thousandths of an inch.

Set	Units											
	3	4	5	6	7	8	9	10	11	12	13	14
14	$2\frac{1}{32}$ 0.0323	$3\frac{3}{32}$ 0.0430	$3\frac{7}{8}$ 0.0538	$4\frac{21}{32}$ 0.0645	$5\frac{7}{16}$ 0.0753	$6\frac{7}{32}$ 0.0861	7 0.0968	$7\frac{25}{32}$ 0.1076	$8\frac{9}{16}$ 0.1184	$9\frac{11}{32}$ 0.1291	$10\frac{1}{8}$ 0.1399	$10\frac{7}{8}$ 0.1506
$14\frac{1}{4}$	$2\frac{3}{8}$ 0.0328	$3\frac{5}{32}$ 0.0438	$3\frac{31}{32}$ 0.0547	$4\frac{3}{4}$ 0.0657	$5\frac{17}{32}$ 0.0766	$6\frac{11}{32}$ 0.0876	$7\frac{1}{8}$ 0.0985	$7\frac{29}{32}$ 0.1095	$8\frac{11}{16}$ 0.1204	$9\frac{1}{2}$ 0.1314	$10\frac{9}{32}$ 0.1423	$11\frac{3}{32}$ 0.1533
$14\frac{1}{2}$	$2\frac{1}{2}$ 0.0334	$3\frac{7}{32}$ 0.0446	$4\frac{1}{32}$ 0.0557	$4\frac{27}{32}$ 0.0668	$5\frac{9}{8}$ 0.0780	$6\frac{7}{16}$ 0.0891	$7\frac{1}{4}$ 0.1003	$8\frac{1}{16}$ 0.1114	$8\frac{7}{8}$ 0.1226	$9\frac{21}{32}$ 0.1337	$10\frac{15}{32}$ 0.1449	$11\frac{9}{32}$ 0.1560
$14\frac{3}{4}$	$2\frac{15}{32}$ 0.0340	$3\frac{9}{32}$ 0.0453	$4\frac{3}{32}$ 0.0567	$4\frac{29}{32}$ 0.0680	$5\frac{23}{32}$ 0.0793	$6\frac{1}{16}$ 0.0907	$7\frac{3}{8}$ 0.1020	$8\frac{3}{16}$ 0.1133	9 0.1247	$9\frac{27}{32}$ 0.1360	$10\frac{21}{32}$ 0.1473	$11\frac{15}{32}$ 0.1587
15	$2\frac{1}{2}$ 0.0346	$3\frac{11}{32}$ 0.0461	$4\frac{5}{32}$ 0.0576	5 0.0692	$5\frac{27}{32}$ 0.0807	$6\frac{31}{32}$ 0.0922	$7\frac{1}{2}$ 0.1037	$8\frac{11}{32}$ 0.1153	$9\frac{5}{32}$ 0.1268	10 0.1383	$10\frac{27}{32}$ 0.1499	$11\frac{21}{32}$ 0.1614
$15\frac{1}{4}$	$2\frac{17}{32}$ 0.0351	$3\frac{3}{8}$ 0.0469	$4\frac{1}{4}$ 0.0586	$5\frac{3}{32}$ 0.0703	$5\frac{15}{16}$ 0.0820	$6\frac{25}{32}$ 0.0938	$7\frac{5}{8}$ 0.1055	$8\frac{15}{32}$ 0.1172	$9\frac{5}{16}$ 0.1289	$10\frac{5}{32}$ 0.1406	11 0.1523	$11\frac{7}{8}$ 0.1641
$15\frac{1}{2}$	$2\frac{19}{32}$ 0.0357	$3\frac{7}{16}$ 0.0476	$4\frac{5}{16}$ 0.0596	$5\frac{5}{32}$ 0.0715	$6\frac{1}{32}$ 0.0834	$6\frac{7}{8}$ 0.0953	$7\frac{3}{4}$ 0.1072	$8\frac{19}{32}$ 0.1191	$9\frac{15}{32}$ 0.1310	$10\frac{11}{32}$ 0.1429	$11\frac{3}{16}$ 0.1548	$12\frac{1}{16}$ 0.1668
$15\frac{3}{4}$	$2\frac{5}{8}$ 0.0363	$3\frac{1}{2}$ 0.0484	$4\frac{3}{8}$ 0.0605	$5\frac{1}{4}$ 0.0726	$6\frac{1}{8}$ 0.0847	7 0.0968	$7\frac{7}{8}$ 0.1089	$8\frac{3}{4}$ 0.1210	$9\frac{5}{8}$ 0.1331	$10\frac{1}{2}$ 0.1452	$11\frac{3}{4}$ 0.1573	$12\frac{1}{4}$ 0.1694
16	$2\frac{21}{32}$ 0.0369	$3\frac{1}{16}$ 0.0492	$4\frac{7}{16}$ 0.0615	$5\frac{11}{32}$ 0.0738	$6\frac{1}{4}$ 0.0861	$7\frac{1}{8}$ 0.0984	8 0.1107	$8\frac{7}{8}$ 0.1230	$9\frac{25}{32}$ 0.1352	$10\frac{21}{32}$ 0.1475	$11\frac{1}{16}$ 0.1598	$12\frac{7}{16}$ 0.1721
$16\frac{1}{4}$	$2\frac{11}{16}$ 0.0374	$3\frac{19}{32}$ 0.0499	$4\frac{1}{2}$ 0.0624	$5\frac{13}{32}$ 0.0749	$6\frac{5}{16}$ 0.0874	$7\frac{3}{32}$ 0.0999	$8\frac{1}{8}$ 0.1124	$9\frac{1}{32}$ 0.1249	$9\frac{15}{16}$ 0.1374	$10\frac{27}{32}$ 0.1498	$11\frac{3}{4}$ 0.1623	$12\frac{21}{32}$ 0.1748
$16\frac{1}{2}$	$2\frac{3}{4}$ 0.0380	$3\frac{21}{32}$ 0.0507	$4\frac{15}{32}$ 0.0634	$5\frac{1}{2}$ 0.0761	$6\frac{13}{32}$ 0.0888	$7\frac{11}{32}$ 0.1014	$8\frac{1}{4}$ 0.1141	$9\frac{5}{32}$ 0.1268	$10\frac{9}{32}$ 0.1395	11 0.1522	$11\frac{29}{32}$ 0.1648	$12\frac{23}{32}$ 0.1775
$16\frac{3}{4}$	$2\frac{25}{32}$ 0.0386	$3\frac{23}{32}$ 0.0515	$4\frac{21}{32}$ 0.0644	$5\frac{9}{16}$ 0.0772	$6\frac{1}{2}$ 0.0901	$7\frac{7}{16}$ 0.1030	$8\frac{3}{8}$ 0.1158	$9\frac{5}{16}$ 0.1287	$10\frac{1}{4}$ 0.1416	$11\frac{5}{32}$ 0.1545	$12\frac{3}{32}$ 0.1673	$13\frac{1}{32}$ 0.1802
17	$2\frac{27}{32}$ 0.0392	$3\frac{25}{32}$ 0.0522	$4\frac{23}{32}$ 0.0653	$5\frac{21}{32}$ 0.0784	$6\frac{19}{32}$ 0.0914	$7\frac{9}{16}$ 0.1045	$8\frac{1}{2}$ 0.1176	$9\frac{7}{16}$ 0.1306	$10\frac{3}{8}$ 0.1437	$11\frac{11}{32}$ 0.1568	$12\frac{5}{32}$ 0.1689	$13\frac{7}{32}$ 0.1829
$17\frac{1}{4}$	$2\frac{7}{8}$ 0.0398	$3\frac{27}{32}$ 0.0530	$4\frac{25}{32}$ 0.0663	$5\frac{3}{4}$ 0.0795	$6\frac{23}{32}$ 0.0928	$7\frac{31}{32}$ 0.1060	$8\frac{5}{8}$ 0.1193	$9\frac{19}{32}$ 0.1326	$10\frac{17}{32}$ 0.1458	$11\frac{1}{2}$ 0.1591	$12\frac{15}{32}$ 0.1723	$13\frac{15}{32}$ 0.1856
$17\frac{1}{2}$	$2\frac{29}{32}$ 0.0403	$3\frac{7}{8}$ 0.0538	$4\frac{7}{8}$ 0.0672	$5\frac{27}{32}$ 0.0807	$6\frac{15}{16}$ 0.0941	$7\frac{25}{32}$ 0.1076	$8\frac{3}{4}$ 0.1210	$9\frac{33}{32}$ 0.1345	$10\frac{11}{16}$ 0.1479	$11\frac{21}{32}$ 0.1614	$12\frac{5}{8}$ 0.1748	$13\frac{5}{8}$ 0.1883
$17\frac{3}{4}$	$2\frac{31}{32}$ 0.0409	$3\frac{15}{16}$ 0.0546	$4\frac{15}{16}$ 0.0682	$5\frac{29}{32}$ 0.0818	$6\frac{29}{32}$ 0.0955	$7\frac{7}{8}$ 0.1091	$8\frac{7}{8}$ 0.1228	$9\frac{27}{32}$ 0.1364	$10\frac{27}{32}$ 0.1500	$11\frac{27}{32}$ 0.1637	$12\frac{13}{16}$ 0.1773	$13\frac{13}{16}$ 0.1910
18	3 0.0415	4 0.0553	5 0.0692	6 0.0830	7 0.0968	8 0.1107	9 0.1245	10 0.1383	11 0.1522	12 0.1660	13 0.1798	14 0.1937
$18\frac{1}{4}$	$3\frac{1}{32}$ 0.0421	$4\frac{1}{16}$ 0.0561	$5\frac{1}{16}$ 0.0701	$6\frac{3}{32}$ 0.0841	$7\frac{3}{32}$ 0.0982	$8\frac{1}{8}$ 0.1122	$9\frac{1}{8}$ 0.1262	$10\frac{1}{8}$ 0.1402	$11\frac{5}{32}$ 0.1543	$12\frac{5}{32}$ 0.1683	$13\frac{3}{16}$ 0.1823	$14\frac{3}{16}$ 0.1963
$18\frac{1}{2}$	$3\frac{3}{32}$ 0.0426	$4\frac{3}{32}$ 0.0569	$5\frac{1}{8}$ 0.0711	$6\frac{5}{32}$ 0.0853	$7\frac{3}{16}$ 0.0995	$8\frac{7}{32}$ 0.1137	$9\frac{1}{4}$ 0.1280	$10\frac{9}{32}$ 0.1422	$11\frac{5}{16}$ 0.1564	$12\frac{11}{32}$ 0.1706	$13\frac{3}{8}$ 0.1848	$14\frac{3}{8}$ 0.1990
$18\frac{3}{4}$	$3\frac{5}{16}$ 0.0432	$4\frac{5}{32}$ 0.0576	$5\frac{3}{8}$ 0.0720	$6\frac{1}{4}$ 0.0865	$7\frac{9}{32}$ 0.1009	$8\frac{13}{32}$ 0.1153	$9\frac{3}{8}$ 0.1297	$10\frac{13}{32}$ 0.1441	$11\frac{15}{32}$ 0.1585	12 0.1729	$13\frac{17}{32}$ 0.1873	$14\frac{19}{32}$ 0.2017

For large composition matrices – 14 set to 18 $\frac{3}{4}$ set – 15 units to 26 units

Set	Units											
	15	16	17	18	19	20	21	22	23	24	25	26
14	$11\frac{21}{32}$ 0.1614	$12\frac{7}{16}$ 0.1722	$13\frac{7}{32}$ 0.1829	14 0.1937	$14\frac{25}{32}$ 0.2044	$15\frac{9}{16}$ 0.2152	$16\frac{11}{32}$ 0.2259	$17\frac{1}{8}$ 0.2367	$17\frac{7}{8}$ 0.2474	$18\frac{21}{32}$ 0.2582	$19\frac{7}{16}$ 0.2690	$20\frac{7}{32}$ 0.2797
14 $\frac{1}{4}$	$11\frac{7}{8}$ 0.1642	$12\frac{21}{32}$ 0.1752	$13\frac{7}{16}$ 0.1861	14$\frac{1}{4}$ 0.1971	$15\frac{1}{32}$ 0.2080	$15\frac{27}{32}$ 0.2190	$16\frac{5}{8}$ 0.2299	$17\frac{13}{32}$ 0.2409	$18\frac{3}{16}$ 0.2518	19 0.2628	$19\frac{25}{32}$ 0.2737	$20\frac{13}{32}$ 0.2847
14 $\frac{1}{2}$	$12\frac{3}{32}$ 0.1671	$12\frac{7}{8}$ 0.1783	$13\frac{11}{16}$ 0.1894	14$\frac{1}{2}$ 0.2006	$15\frac{5}{16}$ 0.2117	$16\frac{3}{32}$ 0.2228	$16\frac{23}{32}$ 0.2340	$17\frac{23}{32}$ 0.2451	$18\frac{7}{32}$ 0.2563	$19\frac{11}{32}$ 0.2674	$20\frac{1}{8}$ 0.2786	$20\frac{15}{16}$ 0.2897
14 $\frac{3}{4}$	$12\frac{9}{32}$ 0.1700	$13\frac{3}{32}$ 0.1813	$13\frac{15}{16}$ 0.1927	14$\frac{3}{4}$ 0.2040	$15\frac{9}{16}$ 0.2154	$16\frac{13}{32}$ 0.2267	$17\frac{7}{32}$ 0.2380	$18\frac{1}{32}$ 0.2494	$18\frac{27}{32}$ 0.2607	$19\frac{21}{32}$ 0.2720	$20\frac{15}{16}$ 0.2834	$21\frac{5}{16}$ 0.2947
15	$12\frac{1}{2}$ 0.1729	$13\frac{11}{32}$ 0.1844	$14\frac{5}{32}$ 0.1960	15 0.2075	$15\frac{27}{32}$ 0.2190	$16\frac{31}{32}$ 0.2305	$17\frac{1}{2}$ 0.2421	$18\frac{11}{32}$ 0.2536	$19\frac{5}{32}$ 0.2651	20 0.2767	$20\frac{27}{32}$ 0.2882	$21\frac{21}{32}$ 0.2997
15 $\frac{1}{4}$	$12\frac{23}{32}$ 0.1758	$13\frac{9}{16}$ 0.1875	$14\frac{13}{32}$ 0.1992	15$\frac{1}{4}$ 0.2110	$16\frac{3}{32}$ 0.2227	$16\frac{15}{16}$ 0.2344	$17\frac{25}{32}$ 0.2461	$18\frac{5}{8}$ 0.2578	$19\frac{15}{32}$ 0.2695	$20\frac{5}{16}$ 0.2813	$21\frac{3}{16}$ 0.2930	$22\frac{1}{32}$ 0.3047
15 $\frac{1}{2}$	$12\frac{29}{32}$ 0.1787	$13\frac{25}{32}$ 0.1906	$14\frac{5}{8}$ 0.2025	15$\frac{1}{2}$ 0.2144	$16\frac{3}{8}$ 0.2263	$17\frac{7}{32}$ 0.2382	$18\frac{3}{32}$ 0.2501	$18\frac{11}{8}$ 0.2621	$19\frac{13}{8}$ 0.2740	$20\frac{21}{32}$ 0.2859	$21\frac{17}{32}$ 0.2978	$22\frac{13}{32}$ 0.3097
15 $\frac{3}{4}$	$13\frac{1}{8}$ 0.1816	14 0.1937	$14\frac{7}{8}$ 0.2058	15$\frac{3}{4}$ 0.2179	$16\frac{5}{8}$ 0.2300	$17\frac{1}{2}$ 0.2421	$18\frac{3}{8}$ 0.2542	$19\frac{1}{4}$ 0.2663	$20\frac{1}{8}$ 0.2784	21 0.2905	$21\frac{7}{8}$ 0.3026	$22\frac{3}{4}$ 0.3147
16	$13\frac{11}{32}$ 0.1844	$14\frac{7}{32}$ 0.1967	$15\frac{3}{32}$ 0.2090	16 0.2213	$16\frac{7}{8}$ 0.2336	$17\frac{25}{32}$ 0.2459	$18\frac{21}{32}$ 0.2582	$19\frac{9}{16}$ 0.2705	$20\frac{7}{16}$ 0.2828	$21\frac{11}{32}$ 0.2951	$22\frac{7}{32}$ 0.3074	$23\frac{3}{32}$ 0.3197
16 $\frac{1}{4}$	$13\frac{17}{32}$ 0.1873	$14\frac{7}{16}$ 0.1998	$15\frac{11}{32}$ 0.2123	16$\frac{1}{4}$ 0.2248	$17\frac{5}{32}$ 0.2373	$18\frac{17}{16}$ 0.2498	$18\frac{31}{32}$ 0.2622	$19\frac{5}{8}$ 0.2747	$20\frac{3}{2}$ 0.2872	$21\frac{21}{32}$ 0.2997	$22\frac{9}{16}$ 0.3122	$23\frac{15}{16}$ 0.3247
16 $\frac{1}{2}$	$13\frac{3}{4}$ 0.1902	$14\frac{21}{32}$ 0.2029	$15\frac{19}{32}$ 0.2156	16$\frac{1}{2}$ 0.2282	$17\frac{13}{32}$ 0.2409	$18\frac{11}{32}$ 0.2536	$19\frac{1}{4}$ 0.2663	$20\frac{5}{32}$ 0.2790	$21\frac{3}{32}$ 0.2916	22 0.3043	$22\frac{25}{32}$ 0.3170	$23\frac{27}{32}$ 0.3297
16 $\frac{3}{4}$	$13\frac{31}{32}$ 0.1931	$14\frac{7}{8}$ 0.2060	$15\frac{13}{16}$ 0.2188	16$\frac{3}{4}$ 0.2317	$17\frac{11}{16}$ 0.2446	$18\frac{19}{32}$ 0.2574	$19\frac{17}{32}$ 0.2703	$20\frac{15}{16}$ 0.2832	$21\frac{13}{32}$ 0.2961	$22\frac{5}{16}$ 0.3089	$23\frac{1}{4}$ 0.3218	$24\frac{3}{16}$ 0.3347
17	$14\frac{5}{32}$ 0.1960	$15\frac{1}{8}$ 0.2090	$16\frac{1}{16}$ 0.2221	17 0.2351	$17\frac{15}{16}$ 0.2482	$18\frac{29}{32}$ 0.2613	$19\frac{27}{32}$ 0.2744	$20\frac{25}{32}$ 0.2874	$21\frac{23}{32}$ 0.3005	$22\frac{11}{16}$ 0.3136	$23\frac{5}{8}$ 0.3266	$24\frac{9}{16}$ 0.3397
17 $\frac{1}{4}$	$14\frac{3}{8}$ 0.1988	$15\frac{11}{32}$ 0.2121	$16\frac{9}{32}$ 0.2254	17$\frac{1}{4}$ 0.2386	$18\frac{7}{32}$ 0.2519	$19\frac{5}{32}$ 0.2651	$20\frac{1}{8}$ 0.2784	$21\frac{3}{32}$ 0.2916	$22\frac{1}{32}$ 0.3049	23 0.3182	$23\frac{31}{32}$ 0.3314	$24\frac{29}{32}$ 0.3447
17 $\frac{1}{2}$	$14\frac{19}{32}$ 0.2017	$15\frac{9}{16}$ 0.2152	$16\frac{17}{32}$ 0.2286	17$\frac{1}{2}$ 0.2421	$18\frac{15}{16}$ 0.2555	$19\frac{7}{16}$ 0.2690	$20\frac{13}{32}$ 0.2824	$21\frac{3}{8}$ 0.2959	$22\frac{3}{8}$ 0.3093	$23\frac{11}{32}$ 0.3228	$24\frac{5}{16}$ 0.3362	$25\frac{9}{32}$ 0.3497
17 $\frac{3}{4}$	$14\frac{13}{16}$ 0.2046	$15\frac{25}{32}$ 0.2182	$16\frac{25}{32}$ 0.2319	17$\frac{3}{4}$ 0.2455	$18\frac{3}{8}$ 0.2592	$19\frac{23}{32}$ 0.2728	$20\frac{23}{32}$ 0.2865	$22\frac{1}{16}$ 0.3001	$22\frac{11}{16}$ 0.3137	$23\frac{21}{32}$ 0.3274	$24\frac{21}{32}$ 0.3410	$25\frac{21}{32}$ 0.3547
18	15 0.2075	16 0.2213	17 0.2352	18 0.2490	19 0.2628	20 0.2767	21 0.2905	22 0.3043	23 0.3182	24 0.3320	25 0.3458	26 0.3596
18 $\frac{1}{4}$	$15\frac{7}{32}$ 0.2104	$16\frac{7}{32}$ 0.2244	$17\frac{1}{4}$ 0.2384	18$\frac{1}{4}$ 0.2524	$19\frac{9}{32}$ 0.2665	$20\frac{9}{32}$ 0.2805	$21\frac{9}{32}$ 0.2945	$22\frac{5}{16}$ 0.3086	$23\frac{5}{16}$ 0.3226	$24\frac{11}{32}$ 0.3366	$25\frac{11}{32}$ 0.3506	$26\frac{3}{8}$ 0.3647
18 $\frac{1}{2}$	$15\frac{13}{32}$ 0.2133	$16\frac{7}{16}$ 0.2275	$17\frac{15}{32}$ 0.2417	18$\frac{1}{2}$ 0.2559	$19\frac{17}{32}$ 0.2701	$20\frac{9}{16}$ 0.2843	$21\frac{13}{32}$ 0.2986	$22\frac{5}{8}$ 0.3128	$23\frac{21}{32}$ 0.3270	$24\frac{21}{32}$ 0.3412	$25\frac{11}{16}$ 0.3554	$26\frac{23}{32}$ 0.3697
18 $\frac{3}{4}$	$15\frac{5}{8}$ 0.2161	$16\frac{11}{16}$ 0.2306	$17\frac{23}{32}$ 0.2450	18$\frac{3}{4}$ 0.2594	$19\frac{13}{16}$ 0.2738	$20\frac{27}{32}$ 0.2882	$21\frac{7}{8}$ 0.3026	$22\frac{23}{32}$ 0.3170	$23\frac{31}{32}$ 0.3314	25 0.3458	$26\frac{1}{32}$ 0.3602	$27\frac{3}{32}$ 0.3746

Micrometer head settings (continued)

For large composition matrices –19 set to 23 $\frac{3}{4}$ set – 3 units to 14 units

Upper figures show adjustment in points and fractions of a point of wedge screw handwheel scale;
lower figures show resultant sizes in thousandths of an inch.

Set	Units											
	3	4	5	6	7	8	9	10	11	12	13	14
19	3 $\frac{5}{32}$ 0.0438	4 $\frac{7}{32}$ 0.0584	5 $\frac{9}{32}$ 0.0730	6 $\frac{11}{32}$ 0.0876	7 $\frac{3}{8}$ 0.1022	8 $\frac{7}{16}$ 0.1168	9$\frac{1}{2}$ 0.1314	10 $\frac{9}{16}$ 0.1460	11 $\frac{11}{32}$ 0.1606	12 $\frac{21}{32}$ 0.1752	13 $\frac{23}{32}$ 0.1898	14 $\frac{25}{32}$ 0.2044
19 $\frac{1}{4}$	3 $\frac{7}{32}$ 0.0444	4 $\frac{9}{32}$ 0.0592	5 $\frac{11}{32}$ 0.0740	6 $\frac{13}{32}$ 0.0888	7 $\frac{15}{32}$ 0.1036	8 $\frac{9}{16}$ 0.1184	9$\frac{5}{8}$ 0.1331	10 $\frac{11}{16}$ 0.1479	11 $\frac{3}{4}$ 0.1627	12 $\frac{27}{32}$ 0.1775	13 $\frac{29}{32}$ 0.1923	14 $\frac{31}{32}$ 0.2071
19 $\frac{1}{2}$	3 $\frac{1}{4}$ 0.0450	4 $\frac{11}{32}$ 0.0599	5 $\frac{13}{32}$ 0.0749	6 $\frac{1}{2}$ 0.0899	7 $\frac{19}{32}$ 0.1049	8 $\frac{21}{32}$ 0.1199	9$\frac{3}{4}$ 0.1349	10 $\frac{27}{32}$ 0.1499	11 $\frac{29}{32}$ 0.1648	13 0.1798	14 $\frac{3}{32}$ 0.1948	15 $\frac{5}{32}$ 0.2098
19 $\frac{3}{4}$	3 $\frac{3}{32}$ 0.0455	4 $\frac{3}{8}$ 0.0607	5 $\frac{15}{32}$ 0.0759	6 $\frac{17}{32}$ 0.0911	7 $\frac{11}{16}$ 0.1062	8 $\frac{25}{32}$ 0.1214	9$\frac{7}{8}$ 0.1366	10 $\frac{31}{32}$ 0.1518	12 $\frac{1}{16}$ 0.1670	13 $\frac{5}{32}$ 0.1821	14 $\frac{1}{4}$ 0.1973	15 $\frac{3}{8}$ 0.2125
20	3 $\frac{11}{32}$ 0.0461	4 $\frac{7}{16}$ 0.0615	5 $\frac{9}{16}$ 0.0769	6 $\frac{31}{32}$ 0.0922	7 $\frac{25}{32}$ 0.1076	8 $\frac{7}{8}$ 0.1230	10 0.1383	11 $\frac{3}{32}$ 0.1537	12 $\frac{7}{32}$ 0.1691	13 $\frac{11}{32}$ 0.1844	14 $\frac{7}{16}$ 0.1998	15 $\frac{9}{16}$ 0.2152
20 $\frac{1}{4}$	3 $\frac{3}{8}$ 0.0467	4 $\frac{1}{2}$ 0.0622	5 $\frac{5}{8}$ 0.0778	6 $\frac{3}{4}$ 0.0934	7 $\frac{7}{8}$ 0.1089	9 0.1245	10$\frac{1}{8}$ 0.1401	11 $\frac{1}{4}$ 0.1556	12 $\frac{3}{8}$ 0.1712	13 $\frac{1}{2}$ 0.1867	14 $\frac{5}{8}$ 0.2023	15 $\frac{3}{4}$ 0.2179
20 $\frac{1}{2}$	3 $\frac{13}{32}$ 0.0473	4 $\frac{9}{16}$ 0.0630	5 $\frac{11}{16}$ 0.0788	6 $\frac{27}{32}$ 0.0945	7 $\frac{31}{32}$ 0.1103	9 $\frac{3}{32}$ 0.1260	10$\frac{1}{4}$ 0.1418	11 $\frac{3}{8}$ 0.1575	12 $\frac{17}{32}$ 0.1733	13 $\frac{31}{32}$ 0.1891	14 $\frac{13}{16}$ 0.2048	15 $\frac{15}{16}$ 0.2206
20 $\frac{3}{4}$	3 $\frac{15}{32}$ 0.0478	4 $\frac{5}{8}$ 0.0638	5 $\frac{3}{4}$ 0.0797	6 $\frac{29}{32}$ 0.0957	8 $\frac{1}{16}$ 0.1116	9 $\frac{7}{32}$ 0.1276	10$\frac{3}{8}$ 0.1435	11 $\frac{17}{32}$ 0.1595	12 $\frac{11}{16}$ 0.1754	13 $\frac{25}{32}$ 0.1914	15 0.2073	16 $\frac{5}{32}$ 0.2233
21	3 $\frac{1}{2}$ 0.0484	4 $\frac{21}{32}$ 0.0646	5 $\frac{23}{32}$ 0.0807	7 0.0968	8 $\frac{5}{32}$ 0.1130	9 $\frac{11}{32}$ 0.1291	10$\frac{1}{2}$ 0.1452	11 $\frac{21}{32}$ 0.1614	12 $\frac{27}{32}$ 0.1775	14 0.1937	15 $\frac{5}{32}$ 0.2098	16 $\frac{11}{32}$ 0.2259
21 $\frac{1}{4}$	3 $\frac{17}{32}$ 0.0490	4 $\frac{23}{32}$ 0.0653	5 $\frac{25}{32}$ 0.0817	7 $\frac{3}{32}$ 0.0980	8 $\frac{1}{4}$ 0.1143	9 $\frac{7}{16}$ 0.1306	10$\frac{5}{8}$ 0.1470	11 $\frac{13}{16}$ 0.1633	13 0.1796	14 $\frac{3}{8}$ 0.1960	15 $\frac{11}{16}$ 0.2123	16 $\frac{17}{16}$ 0.2286
21 $\frac{1}{2}$	3 $\frac{19}{32}$ 0.0496	4 $\frac{25}{32}$ 0.0661	5 $\frac{27}{32}$ 0.0826	7 $\frac{5}{32}$ 0.0991	8 $\frac{3}{8}$ 0.1157	9 $\frac{9}{16}$ 0.1322	10$\frac{3}{4}$ 0.1487	11 $\frac{15}{16}$ 0.1652	13 $\frac{5}{32}$ 0.1818	14 $\frac{11}{32}$ 0.1983	15 $\frac{17}{32}$ 0.2148	16 $\frac{23}{32}$ 0.2313
21 $\frac{3}{4}$	3 $\frac{5}{8}$ 0.0501	4 $\frac{27}{32}$ 0.0669	6 $\frac{1}{32}$ 0.0836	7 $\frac{1}{4}$ 0.1003	8 $\frac{15}{32}$ 0.1170	9 $\frac{21}{32}$ 0.1337	10$\frac{7}{8}$ 0.1504	12 $\frac{3}{32}$ 0.1672	13 $\frac{9}{32}$ 0.1839	14 $\frac{1}{2}$ 0.2006	15 $\frac{23}{32}$ 0.2173	16 $\frac{29}{32}$ 0.2340
22	3 $\frac{21}{32}$ 0.0507	4 $\frac{7}{8}$ 0.0676	6 $\frac{3}{32}$ 0.0845	7 $\frac{11}{32}$ 0.1014	8 $\frac{9}{16}$ 0.1183	9 $\frac{25}{32}$ 0.1353	11 0.1522	12 $\frac{7}{32}$ 0.1691	13 $\frac{7}{16}$ 0.1860	14 $\frac{21}{32}$ 0.2029	15 $\frac{7}{8}$ 0.2198	17 $\frac{3}{32}$ 0.2367
22 $\frac{1}{4}$	3 $\frac{23}{32}$ 0.0513	4 $\frac{15}{16}$ 0.0684	6 $\frac{5}{16}$ 0.0855	7 $\frac{13}{32}$ 0.1026	8 $\frac{31}{32}$ 0.1197	9 $\frac{7}{8}$ 0.1368	11$\frac{1}{8}$ 0.1539	12 $\frac{3}{8}$ 0.1710	13 $\frac{19}{32}$ 0.1881	14 $\frac{27}{32}$ 0.2052	16 $\frac{1}{16}$ 0.2223	17 $\frac{5}{16}$ 0.2394
22 $\frac{1}{2}$	3 $\frac{25}{32}$ 0.0519	5 0.0692	6 $\frac{1}{4}$ 0.0865	7 $\frac{1}{2}$ 0.1038	8 $\frac{3}{4}$ 0.1210	10 0.1383	11$\frac{1}{4}$ 0.1556	12 $\frac{1}{2}$ 0.1729	13 $\frac{3}{4}$ 0.1902	15 0.2075	16 $\frac{1}{4}$ 0.2248	17 $\frac{1}{2}$ 0.2421
22 $\frac{3}{4}$	3 $\frac{27}{32}$ 0.0524	4 $\frac{11}{16}$ 0.0699	6 $\frac{15}{16}$ 0.0874	7 $\frac{19}{32}$ 0.1049	8 $\frac{27}{32}$ 0.1224	10 $\frac{1}{8}$ 0.1399	11$\frac{3}{8}$ 0.1574	12 $\frac{21}{32}$ 0.1748	13 $\frac{25}{32}$ 0.1923	15 $\frac{5}{32}$ 0.2098	16 $\frac{7}{16}$ 0.2273	17 $\frac{11}{16}$ 0.2448
23	3 $\frac{29}{32}$ 0.0530	5 $\frac{3}{32}$ 0.0707	6 $\frac{3}{8}$ 0.0884	7 $\frac{21}{32}$ 0.1061	8 $\frac{15}{16}$ 0.1237	10 $\frac{7}{32}$ 0.1414	11$\frac{1}{2}$ 0.1591	12 $\frac{25}{32}$ 0.1768	14 $\frac{1}{16}$ 0.1944	15 $\frac{11}{32}$ 0.2121	16 $\frac{5}{8}$ 0.2298	17 $\frac{25}{32}$ 0.2475
23 $\frac{1}{4}$	3 $\frac{7}{8}$ 0.0536	5 $\frac{5}{32}$ 0.0715	6 $\frac{15}{32}$ 0.0893	7 $\frac{3}{4}$ 0.1072	9 $\frac{1}{32}$ 0.1251	10 $\frac{13}{32}$ 0.1429	11$\frac{5}{8}$ 0.1608	12 $\frac{29}{32}$ 0.1787	14 $\frac{3}{32}$ 0.1965	15 $\frac{1}{2}$ 0.2144	16 $\frac{25}{32}$ 0.2323	18 $\frac{3}{32}$ 0.2502
23 $\frac{1}{2}$	3 $\frac{31}{32}$ 0.0542	5 $\frac{7}{32}$ 0.0722	6 $\frac{17}{32}$ 0.0903	7 $\frac{27}{32}$ 0.1084	9 $\frac{1}{8}$ 0.1264	10 $\frac{7}{16}$ 0.1445	11$\frac{3}{4}$ 0.1625	13 $\frac{1}{16}$ 0.1806	14 $\frac{3}{8}$ 0.1987	15 $\frac{21}{32}$ 0.2167	16 $\frac{31}{32}$ 0.2348	18 $\frac{9}{32}$ 0.2528
23 $\frac{3}{4}$	3 $\frac{33}{32}$ 0.0548	5 $\frac{9}{32}$ 0.0730	6 $\frac{19}{32}$ 0.0913	7 $\frac{29}{32}$ 0.1095	9 $\frac{1}{4}$ 0.1278	10 $\frac{9}{16}$ 0.1460	11$\frac{7}{8}$ 0.1643	13 $\frac{3}{16}$ 0.1825	14 $\frac{1}{2}$ 0.2008	15 $\frac{27}{32}$ 0.2190	17 $\frac{5}{32}$ 0.2373	18 $\frac{15}{32}$ 0.2555

For large composition matrices – 19 set to $23\frac{3}{4}$ set – 15 units to 26 units

Set	Units											
	15	16	17	18	19	20	21	22	23	24	25	26
19	$15\frac{3}{2}$ 0.2190	$16\frac{7}{8}$ 0.2336	$17\frac{15}{16}$ 0.2482	19 0.2628	$20\frac{1}{16}$ 0.2774	$21\frac{3}{32}$ 0.2920	$22\frac{5}{32}$ 0.3066	$23\frac{7}{32}$ 0.3212	$24\frac{9}{32}$ 0.3358	$25\frac{11}{32}$ 0.3504	$26\frac{3}{8}$ 0.3650	$27\frac{7}{16}$ 0.3796
$19\frac{1}{4}$	$16\frac{1}{32}$ 0.2219	$17\frac{3}{32}$ 0.2367	$18\frac{3}{16}$ 0.2515	$19\frac{1}{4}$ 0.2663	$20\frac{5}{16}$ 0.2811	$21\frac{3}{8}$ 0.2959	$22\frac{15}{32}$ 0.3107	$23\frac{17}{32}$ 0.3255	$24\frac{19}{32}$ 0.3403	$25\frac{21}{32}$ 0.3551	$26\frac{23}{32}$ 0.3700	$27\frac{1}{8}$ 0.3856
$19\frac{1}{2}$	$16\frac{1}{4}$ 0.2248	$17\frac{11}{32}$ 0.2398	$18\frac{13}{32}$ 0.2548	$19\frac{1}{2}$ 0.2697	$20\frac{13}{32}$ 0.2847	$21\frac{21}{32}$ 0.2997	$22\frac{3}{4}$ 0.3147	$23\frac{27}{32}$ 0.3297	$24\frac{29}{32}$ 0.3447	26 0.3597	$27\frac{3}{32}$ 0.3747	$28\frac{5}{32}$ 0.3896
$19\frac{3}{4}$	$16\frac{15}{32}$ 0.2277	$17\frac{9}{16}$ 0.2429	$18\frac{21}{32}$ 0.2580	$19\frac{3}{4}$ 0.2732	$20\frac{27}{32}$ 0.2884	$21\frac{15}{16}$ 0.3036	$23\frac{1}{32}$ 0.3187	$24\frac{5}{32}$ 0.3339	$25\frac{1}{2}$ 0.3491	$26\frac{11}{32}$ 0.3643	$27\frac{7}{16}$ 0.3795	
20	$16\frac{11}{16}$ 0.2306	$17\frac{25}{32}$ 0.2459	$18\frac{33}{32}$ 0.2613	20 0.2767	$21\frac{1}{16}$ 0.2920	$22\frac{7}{32}$ 0.3074	$23\frac{11}{32}$ 0.3228	$24\frac{7}{16}$ 0.3381	$25\frac{9}{16}$ 0.3535	$26\frac{21}{32}$ 0.3689	$27\frac{25}{32}$ 0.3843	
$20\frac{1}{2}$	$16\frac{7}{8}$ 0.2334	18 0.2490	$19\frac{1}{8}$ 0.2646	$20\frac{1}{2}$ 0.2801	$21\frac{3}{8}$ 0.2957	$22\frac{1}{2}$ 0.3112	$23\frac{5}{8}$ 0.3268	$24\frac{3}{4}$ 0.3424	$25\frac{7}{8}$ 0.3579	27 0.3735	$28\frac{1}{8}$ 0.3891	
$20\frac{1}{4}$	$17\frac{3}{32}$ 0.2363	$18\frac{7}{32}$ 0.2521	$19\frac{3}{8}$ 0.2678	$20\frac{1}{4}$ 0.2836	$21\frac{21}{32}$ 0.2993	$22\frac{25}{32}$ 0.3151	$23\frac{29}{32}$ 0.3308	$25\frac{1}{16}$ 0.3466	$26\frac{5}{16}$ 0.3624	$27\frac{9}{16}$ 0.3781		
$20\frac{3}{4}$	$17\frac{9}{32}$ 0.2392	$18\frac{7}{16}$ 0.2551	$19\frac{19}{32}$ 0.2711	$20\frac{3}{4}$ 0.2870	$21\frac{29}{32}$ 0.3030	$23\frac{1}{16}$ 0.3189	$24\frac{7}{32}$ 0.3349	$25\frac{3}{8}$ 0.3509	$26\frac{1}{2}$ 0.3668	$27\frac{21}{32}$ 0.3827		
21	$17\frac{1}{2}$ 0.2421	$18\frac{21}{32}$ 0.2582	$19\frac{27}{32}$ 0.2744	21 0.2905	$22\frac{5}{32}$ 0.3066	$23\frac{11}{32}$ 0.3228	$24\frac{1}{2}$ 0.3389	$25\frac{21}{32}$ 0.3551	$26\frac{27}{32}$ 0.3712	28 0.3873		
$21\frac{1}{4}$	$17\frac{33}{32}$ 0.2450	$18\frac{29}{32}$ 0.2613	$20\frac{1}{16}$ 0.2776	$21\frac{1}{4}$ 0.2940	$22\frac{7}{16}$ 0.3103	$23\frac{3}{8}$ 0.3266	$24\frac{25}{32}$ 0.3430	$25\frac{31}{32}$ 0.3593	$27\frac{3}{32}$ 0.3756			
$21\frac{1}{2}$	$17\frac{29}{32}$ 0.2478	$19\frac{1}{8}$ 0.2644	$20\frac{1}{16}$ 0.2809	$21\frac{1}{2}$ 0.2974	$22\frac{11}{16}$ 0.3139	$23\frac{7}{8}$ 0.3305	$25\frac{3}{32}$ 0.3470	$26\frac{9}{32}$ 0.3635	$27\frac{15}{32}$ 0.3800			
$21\frac{3}{4}$	$18\frac{1}{8}$ 0.2507	$19\frac{11}{32}$ 0.2674	$20\frac{17}{32}$ 0.2842	$21\frac{3}{4}$ 0.3009	$22\frac{21}{32}$ 0.3176	$24\frac{5}{32}$ 0.3343	$25\frac{3}{8}$ 0.3510	$26\frac{13}{32}$ 0.3677	$27\frac{25}{32}$ 0.3845			
22	$18\frac{11}{32}$ 0.2536	$19\frac{9}{16}$ 0.2705	$20\frac{25}{32}$ 0.2874	22 0.3043	$23\frac{7}{32}$ 0.3212	$24\frac{7}{16}$ 0.3381	$25\frac{21}{32}$ 0.3550	$26\frac{7}{8}$ 0.3720				
$22\frac{1}{4}$	$18\frac{17}{32}$ 0.2565	$19\frac{25}{32}$ 0.2736	21 0.2907	$22\frac{1}{4}$ 0.3078	$23\frac{15}{32}$ 0.3249	$24\frac{23}{32}$ 0.3420	$25\frac{31}{32}$ 0.3591	$27\frac{3}{16}$ 0.3762				
$22\frac{1}{2}$	$18\frac{3}{4}$ 0.2594	20 0.2767	$21\frac{1}{2}$ 0.2940	$22\frac{1}{2}$ 0.3112	$23\frac{1}{4}$ 0.3285	25 0.3458	$26\frac{1}{4}$ 0.3631	$27\frac{1}{2}$ 0.3804				
$22\frac{3}{4}$	$18\frac{31}{32}$ 0.2662	$20\frac{7}{32}$ 0.2797	$21\frac{15}{32}$ 0.2972	$22\frac{3}{4}$ 0.3147	24 0.3322	$25\frac{9}{32}$ 0.3497	$26\frac{17}{32}$ 0.3672	$27\frac{11}{8}$ 0.3846				
23	$19\frac{5}{32}$ 0.2651	$20\frac{7}{16}$ 0.2828	$21\frac{23}{32}$ 0.3005	23 0.3182	$24\frac{9}{32}$ 0.3358	$25\frac{9}{16}$ 0.3535	$26\frac{27}{32}$ 0.3712	$28\frac{1}{8}$ 0.3889				
$23\frac{1}{4}$	$19\frac{3}{8}$ 0.2680	$20\frac{21}{32}$ 0.2859	$21\frac{31}{32}$ 0.3038	$23\frac{1}{4}$ 0.3216	$24\frac{17}{32}$ 0.3395	$25\frac{27}{32}$ 0.3574	$27\frac{1}{8}$ 0.3752					
$23\frac{1}{2}$	$19\frac{19}{32}$ 0.2709	$20\frac{7}{8}$ 0.2890	$22\frac{3}{16}$ 0.3070	$23\frac{1}{2}$ 0.3251	$24\frac{11}{8}$ 0.3431	$26\frac{3}{32}$ 0.3612	$27\frac{13}{32}$ 0.3793					
$23\frac{3}{4}$	$19\frac{25}{32}$ 0.2738	$21\frac{3}{32}$ 0.2920	$22\frac{7}{16}$ 0.3103	$23\frac{3}{4}$ 0.3285	$25\frac{1}{16}$ 0.3468	$26\frac{3}{8}$ 0.3650	$27\frac{23}{32}$ 0.3833					

Micrometer head settings

For display matrices

Width in points denotes the micrometer head setting

Matrix marking		Matrix marking		Matrix marking		Matrix marking												
Width in points	Old style	Width in points	Old style	Width in points	Old style	Width in points	Old style	Width in points	Width in inches	Width in points	Width in inches	Width in points	Width in inches	Width in points	Width in inches			
2		0-0277	15	*14 8	0-2075	28	10 8	0-3873	41	** 6 8	0-5671	54	0-7470	67	0-9268	80	1-1066	
2 $\frac{1}{2}$	*	2 2	0-0311	15 $\frac{1}{2}$	*15 2	0-2110	28 $\frac{1}{2}$	11 2	0-3908	41 $\frac{1}{2}$	** 7 2	0-5706	54 $\frac{1}{2}$	0-7505	67 $\frac{1}{2}$	0-9303	80 $\frac{1}{2}$	1-1101
2 $\frac{3}{4}$	*	2 4	0-0346	15 $\frac{3}{4}$	*15 4	0-2144	28 $\frac{3}{4}$	11 4	0-3943	41 $\frac{3}{4}$	** 7 4	0-5741	54 $\frac{3}{4}$	0-7539	67 $\frac{3}{4}$	0-9337	80 $\frac{3}{4}$	1-1136
3	*	2 6	0-0380	16	*15 6	0-2179	29	11 6	0-3977	42	** 7 6	0-5775	54 $\frac{1}{2}$	0-7574	67 $\frac{1}{2}$	0-9372	80 $\frac{1}{2}$	1-1170
3 $\frac{1}{4}$	*	2 8	0-0415	16 $\frac{1}{4}$	*16 8	0-2213	29 $\frac{1}{4}$	11 8	0-4012	42 $\frac{1}{4}$	** 7 8	0-5810	55	0-7608	68	0-9406	81	1-1205
3 $\frac{1}{2}$	*	3 2	0-0450	16 $\frac{1}{2}$	*16 2	0-2248	29 $\frac{1}{2}$	12 2	0-4046	42 $\frac{1}{2}$	** 8 2	0-5844	55 $\frac{1}{2}$	0-7643	68 $\frac{1}{2}$	0-9441	81 $\frac{1}{2}$	1-1240
3 $\frac{3}{4}$	*	3 4	0-0484	16 $\frac{3}{4}$	*16 4	0-2283	29 $\frac{3}{4}$	12 4	0-4081	42 $\frac{3}{4}$	** 8 4	0-5879	55 $\frac{3}{4}$	0-7677	68 $\frac{3}{4}$	0-9476	81 $\frac{3}{4}$	1-1274
4	*	3 6	0-0519	17	*16 6	0-2317	29 $\frac{3}{4}$	12 6	0-4115	43	** 8 6	0-5913	55 $\frac{3}{4}$	0-7712	68 $\frac{3}{4}$	0-9510	81 $\frac{3}{4}$	1-1309
4 $\frac{1}{4}$	*	3 8	0-0553	17 $\frac{1}{4}$	*17 8	0-2352	30	12 8	0-4150	43 $\frac{1}{4}$	** 8 8	0-5948	56	0-7746	69	0-9545	82	1-1343
4 $\frac{1}{2}$	*	4 2	0-0588	17 $\frac{1}{2}$	*17 2	0-2386	30 $\frac{1}{2}$	13 2	0-4185	43 $\frac{1}{2}$	** 9 2	0-5983	56 $\frac{1}{2}$	0-7781	69 $\frac{1}{2}$	0-9579	82 $\frac{1}{2}$	1-1378
4 $\frac{3}{4}$	*	4 4	0-0623	17 $\frac{3}{4}$	*17 4	0-2421	30 $\frac{3}{4}$	13 4	0-4219	43 $\frac{3}{4}$	** 9 4	0-6017	56 $\frac{3}{4}$	0-7816	69 $\frac{3}{4}$	0-9614	82 $\frac{3}{4}$	1-1412
5	*	4 6	0-0657	18	*17 6	0-2455	31	13 6	0-4254	44	** 9 6	0-6052	56 $\frac{3}{4}$	0-7850	69 $\frac{3}{4}$	0-9649	82 $\frac{3}{4}$	1-1447
5 $\frac{1}{4}$	*	4 8	0-0692	18 $\frac{1}{4}$	*18 8	0-2490	31 $\frac{1}{4}$	13 8	0-4288	44 $\frac{1}{4}$	** 9 8	0-6086	57	0-7885	70	0-9683	83	1-1481
5 $\frac{1}{2}$	*	5 2	0-0726	18 $\frac{1}{2}$	*18 2	0-2525	31 $\frac{1}{2}$	14 2	0-4323	44 $\frac{1}{2}$	** 10 2	0-6121	57 $\frac{1}{2}$	0-7919	70 $\frac{1}{2}$	0-9718	83 $\frac{1}{2}$	1-1516
5 $\frac{3}{4}$	*	5 4	0-0761	18 $\frac{3}{4}$	*18 4	0-2559	31 $\frac{3}{4}$	14 4	0-4358	44 $\frac{3}{4}$	** 10 4	0-6156	57 $\frac{3}{4}$	0-7954	70 $\frac{3}{4}$	0-9752	83 $\frac{3}{4}$	1-1551
6	*	5 6	0-0795	19	*18 6	0-2594	32	14 6	0-4392	45	** 10 6	0-6190	57 $\frac{3}{4}$	0-7989	70 $\frac{3}{4}$	0-9787	83 $\frac{3}{4}$	1-1585
6 $\frac{1}{4}$	*	5 8	0-0830	19 $\frac{1}{4}$	*19 8	0-2628	32 $\frac{1}{4}$	14 8	0-4427	45 $\frac{1}{4}$	** 10 8	0-6225	58	0-8023	71	0-9821	84	1-1620
6 $\frac{1}{2}$	*	6 2	0-0865	19 $\frac{1}{2}$	*2 2	0-2663	32 $\frac{1}{2}$	15 2	0-4461	45 $\frac{1}{2}$	** 11 2	0-6259	58 $\frac{1}{2}$	0-8058	71 $\frac{1}{2}$	0-9856	84 $\frac{1}{2}$	1-1655
6 $\frac{3}{4}$	*	6 4	0-0899	19 $\frac{3}{4}$	*2 4	0-2698	32 $\frac{3}{4}$	15 4	0-4496	45 $\frac{3}{4}$	** 11 4	0-6294	58 $\frac{3}{4}$	0-8092	71 $\frac{3}{4}$	0-9891	84 $\frac{3}{4}$	1-1689
7	*	6 6	0-0934	20	*2 6	0-2732	33	15 6	0-4530	46	** 11 6	0-6328	58 $\frac{3}{4}$	0-8127	71 $\frac{3}{4}$	0-9925	84 $\frac{3}{4}$	1-1724
7 $\frac{1}{4}$	*	6 8	0-0968	20 $\frac{1}{4}$	*2 8	0-2767	33 $\frac{1}{4}$	15 8	0-4565	46 $\frac{1}{4}$	** 11 8	0-6363	59	0-8161	72	0-9960	85	1-1758
7 $\frac{1}{2}$	*	7 2	0-1003	20 $\frac{1}{2}$	*3 2	0-2801	33 $\frac{1}{2}$	16 2	0-4600	46 $\frac{1}{2}$	** 12 2	0-6398	59 $\frac{1}{2}$	0-8196	72 $\frac{1}{2}$	0-9994	85 $\frac{1}{2}$	1-1793
7 $\frac{3}{4}$	*	7 4	0-1038	20 $\frac{3}{4}$	*3 4	0-2836	33 $\frac{3}{4}$	16 4	0-4634	46 $\frac{3}{4}$	** 12 4	0-6432	59 $\frac{3}{4}$	0-8231	72 $\frac{3}{4}$	1-0029	85 $\frac{3}{4}$	1-1827
8	*	7 6	0-1072	21	*3 6	0-2870	34	16 6	0-4669	47	** 12 6	0-6467	59 $\frac{3}{4}$	0-8265	72 $\frac{3}{4}$	1-0064	85 $\frac{3}{4}$	1-1862
8 $\frac{1}{4}$	*	7 8	0-1107	21 $\frac{1}{4}$	*4 8	0-2905	34 $\frac{1}{4}$	16 8	0-4703	47 $\frac{1}{4}$	** 12 8	0-6501	60	0-8300	73	1-0098	86	1-1896
8 $\frac{1}{2}$	*	8 2	0-1141	21 $\frac{1}{2}$	*4 2	0-2940	34 $\frac{1}{2}$	17 2	0-4738	47 $\frac{1}{2}$	** 13 2	0-6536	60 $\frac{1}{2}$	0-8335	73 $\frac{1}{2}$	1-0133	86 $\frac{1}{2}$	1-1931
8 $\frac{3}{4}$	*	8 4	0-1176	21 $\frac{3}{4}$	*4 4	0-2974	34 $\frac{3}{4}$	17 4	0-4773	47 $\frac{3}{4}$	** 13 4	0-6571	60 $\frac{3}{4}$	0-8369	73 $\frac{3}{4}$	1-0167	86 $\frac{3}{4}$	1-1966
9	*	8 6	0-1210	22	*4 6	0-3009	35	17 6	0-4807	48	** 13 6	0-6605	60 $\frac{3}{4}$	0-8404	73 $\frac{3}{4}$	1-0202	86 $\frac{3}{4}$	1-2000
9 $\frac{1}{4}$	*	8 8	0-1245	22 $\frac{1}{4}$	*4 8	0-3043	35 $\frac{1}{4}$	17 8	0-4842	48 $\frac{1}{4}$	** 13 8	0-6640	61	0-8438	74	1-0236	87	1-2035
9 $\frac{1}{2}$	*	9 2	0-1280	22 $\frac{1}{2}$	*5 2	0-3078	35 $\frac{1}{2}$	18 2	0-4876	48 $\frac{1}{2}$	** 13 8	0-6674	61 $\frac{1}{2}$	0-8473	74 $\frac{1}{2}$	1-0271	87 $\frac{1}{2}$	1-2069
9 $\frac{3}{4}$	*	9 4	0-1314	22 $\frac{3}{4}$	*5 4	0-3113	35 $\frac{3}{4}$	18 4	0-4911	48 $\frac{3}{4}$	** 13 8	0-6709	61 $\frac{3}{4}$	0-8507	74 $\frac{3}{4}$	1-0306	87 $\frac{3}{4}$	1-2104
10	*	9 6	0-1349	23	*5 6	0-3147	36	18 6	0-4945	49	** 13 8	0-6743	61 $\frac{3}{4}$	0-8542	74 $\frac{3}{4}$	1-0340	87 $\frac{3}{4}$	1-2139
10 $\frac{1}{4}$	*	9 8	0-1383	23 $\frac{1}{4}$	*6 8	0-3182	36 $\frac{1}{4}$	18 8	0-4980	49 $\frac{1}{4}$	** 13 8	0-6778	62	0-8576	75	1-0375	88	1-2173
10 $\frac{1}{2}$	*	10 2	0-1418	23 $\frac{1}{2}$	*6 2	0-3216	36 $\frac{1}{2}$	** 2 2	0-5014	49 $\frac{1}{2}$	** 13 8	0-6813	62 $\frac{1}{2}$	0-8611	75 $\frac{1}{2}$	1-0409	88 $\frac{1}{2}$	1-2208
10 $\frac{3}{4}$	*	10 4	0-1453	23 $\frac{3}{4}$	*6 4	0-3251	36 $\frac{3}{4}$	** 2 4	0-5049	49 $\frac{3}{4}$	** 13 8	0-6847	62 $\frac{3}{4}$	0-8646	75 $\frac{3}{4}$	1-0444	88 $\frac{3}{4}$	1-2242
11	*	10 6	0-1487	24	*6 6	0-3285	37	** 2 6	0-5083	49 $\frac{3}{4}$	** 13 8	0-6882	62 $\frac{3}{4}$	0-8680	75 $\frac{3}{4}$	1-0479	88 $\frac{3}{4}$	1-2277
11 $\frac{1}{4}$	*	10 8	0-1522	24 $\frac{1}{4}$	*7 8	0-3320	37 $\frac{1}{4}$	** 2 8	0-5118	50	** 13 8	0-6916	63	0-8715	76	1-0513	89	1-2311
11 $\frac{1}{2}$	*	11 2	0-1556	24 $\frac{1}{2}$	*7 2	0-3355	37 $\frac{1}{2}$	** 3 2	0-5153	50 $\frac{1}{2}$	** 13 8	0-6952	63 $\frac{1}{2}$	0-8749	76 $\frac{1}{2}$	1-0548	89 $\frac{1}{2}$	1-2346
11 $\frac{3}{4}$	*	11 4	0-1591	24 $\frac{3}{4}$	*7 4	0-3389	37 $\frac{3}{4}$	** 3 4	0-5187	50 $\frac{3}{4}$	** 13 8	0-6986	63 $\frac{3}{4}$	0-8784	76 $\frac{3}{4}$	1-0582	89 $\frac{3}{4}$	1-2381
12	*	11 6	0-1625	25	*7 6	0-3424	38	** 3 6	0-5222	50 $\frac{3}{4}$	** 13 8	0-7021	63 $\frac{3}{4}$	0-8819	76 $\frac{3}{4}$	1-0617	89 $\frac{3}{4}$	1-2415
12 $\frac{1}{4}$	*	11 8	0-1660	25 $\frac{1}{4}$	*8 8	0-3458	38 $\frac{1}{4}$	** 3 8	0-5256	51	** 13 8	0-7055	64	0-8853	77	1-0651	90	1-2450
12 $\frac{1}{2}$	*	12 2	0-1695	25 $\frac{1}{2}$	*8 2	0-3493	38 $\frac{1}{2}$	** 4 2	0-5291	51 $\frac{1}{2}$	** 13 8	0-7090	64 $\frac{1}{2}$	0-8888	77 $\frac{1}{2}$	1-0686	90 $\frac{1}{2}$	1-2484
12 $\frac{3}{4}$	*	12 4	0-1729	25 $\frac{3}{4}$	*8 4	0-3528	38 $\frac{3}{4}$	** 4 4	0-5326	51 $\frac{3}{4}$	** 13 8	0-7125	64 $\frac{3}{4}$	0-8922	77 $\frac{3}{4}$	1-0721	90 $\frac{3}{4}$	1-2519
13	*	12 6	0-1764	26	*8 6	0-3562	39	** 4 6	0-5360	51 $\frac{3}{4}$	** 13 8	0-7159	64 $\frac{3}{4}$	0-8957	77 $\frac{3}{4}$	1-0755	90 $\frac{3}{4}$	1-2554
13 $\frac{1}{4}$	*	12 8	0-1798	26 $\frac{1}{4}$	*8 8	0-3597	39 $\frac{1}{4}$	** 4 8	0-5395	52	** 13 8	0-7194	65	0-8991	78	1-0790		
13 $\frac{1}{2}$	*	13 2	0-1833	26 $\frac{1}{2}$	*9 2	0-3631	39 $\frac{1}{2}$	** 5 2	0-5429	52 $\frac{1}{2}$	** 13 8	0-7228	65 $\frac{1}{2}$	0-9026	78 $\frac{1}{2}$	1-0824		
13 $\frac{3}{4}$	*	13 4	0-1868	26 $\frac{3}{4}$	*9 4	0-3666	39 $\frac{3}{4}$	** 5 4	0-5464	52 $\frac{3}{4}$	** 13 8	0-7263	65 $\frac{3}{4}$	0-9061	78 $\frac{3}{4}$	1-0859		
14	*	13 6	0-1902	27	*9 6	0-3700	40	** 5 6	0-5498	52 $\frac{3}{4}$	** 13 8	0-7297	65 $\frac{3}{4}$	0-9095	78 $\frac{3}{4}$	1-0894		
14 $\frac{1}{4}$	*	13 8	0-1937	27 $\frac{1}{4}$	*9 8	0-3735	40 $\frac{1}{4}$	** 6 2	0-5533	53	** 13 8	0-7332	66	0-9130	79	1-0928		
14 $\frac{1}{2}$	*	14 2	0-1971	27 $\frac{1}{2}$	*10 2	0-3770	40 $\frac{1}{2}$	** 6 2	0-5568	53 $\frac{1}{2}$	** 13 8	0-7366	66 $\frac{1}{2}$	0-9164	79 $\frac{1}{2}$	1-0963		
14 $\frac{3}{4}$	*	14 4	0-2006	27 $\frac{3}{4}$	*10 4	0-3804	40 $\frac{3}{4}$	** 6 4	0-5602	53 $\frac{3}{4}$	** 13 8	0-7401	66 $\frac{3}{4}$	0-9199	79 $\frac{3}{4}$	1-0997		
15	*	14 6	0-2040	28	*10 6	0-3839	41	** 6 6	0-5637	53 $\frac{3}{4}$	** 13 8	0-7435	66 $\frac{3}{4}$	0-9234	79 $\frac{3}{4}$	1-1032		

Moulds and matrix holders

For use when casting type

	Size		Size	
	5 pt to 12 pt	5 pt to 12 pt	14 pt to 24 pt	14 pt to 48 pt
Moulds	Composition. Use adaptor plate	Composition. Use adaptor plate	Composition (large type) with interchangeable insets. Use adaptor plate	Display, 14 pt to 36 pt and 42 pt to 48 pt. Either kind fitted with interchangeable insets. Use adaptor plate
Mould high space height	0-868"	0-868"	0-868"	0-868"
Matrix	Composition (0-2"×0-2")	Composition (0-2" extended)	Composition (large type, 0-4"×0-2" and 0-4"×0-4")	Display (1"×1", 1"×1 $\frac{1}{8}$ ", 1"×1-35")
Matrix drive	0-050"	0-050"	0-050"	0-050"
Matrix holder	Xa3SL	Xa4SL	Xa5SL	Xa6SL
Mould blade fork*	12SL assd	12SL assd	12SL assd	14 pt to 36 pt 12SL assd 42 pt to 48 pt X32SL
Water block	30SLL	30SLL	30SLL	30SLL
Oiler	a29SL1	a29SL1	a15SL1	a15SL1
Head	Composition	Composition	Display	Display

*When casting type from 5 point to 36 point with the old-style low quad arrangement, use Mould blade fork, X26SL

	Size		
	14 pt to 36 pt	14 pt to 36 pt	42 pt to 72 pt
Moulds	Display. Fitted with interchangeable insets. Use adaptor plate	Super type. Fitted with interchangeable insets	Super type. Fitted with interchangeable insets
Mould high space height	0-868"	0-868"	0-853"
Matrix	Display. American Electrotype (1 $\frac{1}{8}$ "× $\frac{3}{4}$ ")	Display (1"×1")	Display (1 $\frac{1}{8}$ "×1 $\frac{1}{8}$ ", 1 $\frac{1}{8}$ "×1-35")
Matrix drive	0-050"	0-050"	0-065"
Matrix holder	X33SL	Xa6SL	Xa7SL
Mould blade fork*	12SL assd	12SL assd	13SL assd
Water block	30SLL	19SLL	20SLL
Oiler	a15SL1	a15SL1	16SL1
Head	Display	Display	Display

*When casting type from 5 point to 36 point with the old-style low quad arrangement, use Mould blade fork, X26SL

Strip casting correction

Adjustment figures per cast

Overall difference in points	Total number of casts in strip											
	2	3	4	5	6	7	8	9	10	11	12	13
$\frac{1}{2}$	$\frac{1}{4}$ 0.0035	$\frac{5}{32}$ 0.0023	$\frac{1}{8}$ 0.0017	$\frac{3}{32}$ 0.0014	$\frac{3}{32}$ 0.0012	$\frac{1}{16}$ 0.0010	$\frac{1}{16}$ 0.0009	$\frac{1}{16}$ 0.0008	$\frac{1}{16}$ 0.0007	$\frac{1}{32}$ 0.0006	$\frac{1}{32}$ 0.0006	$\frac{1}{32}$ 0.0005
1	$\frac{1}{2}$ 0.0069	$\frac{11}{32}$ 0.0046	$\frac{1}{4}$ 0.0034	$\frac{7}{32}$ 0.0028	$\frac{5}{32}$ 0.0023	$\frac{5}{32}$ 0.0020	$\frac{1}{8}$ 0.0017	$\frac{3}{32}$ 0.0015	$\frac{3}{32}$ 0.0014	$\frac{3}{32}$ 0.0012	$\frac{3}{32}$ 0.0011	$\frac{1}{16}$ 0.0010
2	1 0.0138	$\frac{21}{32}$ 0.0092	$\frac{1}{2}$ 0.0069	$\frac{13}{32}$ 0.0056	$\frac{11}{32}$ 0.0046	$\frac{9}{32}$ 0.0040	$\frac{1}{4}$ 0.0035	$\frac{7}{32}$ 0.0030	$\frac{7}{32}$ 0.0028	$\frac{1}{16}$ 0.0025	$\frac{5}{32}$ 0.0023	$\frac{5}{32}$ 0.0021
3	$1\frac{1}{2}$ 0.0207	1 0.0138	$\frac{3}{4}$ 0.0103	$\frac{13}{32}$ 0.0084	$\frac{1}{2}$ 0.0069	$\frac{7}{16}$ 0.0059	$\frac{3}{8}$ 0.0052	$\frac{11}{32}$ 0.0046	$\frac{5}{16}$ 0.0042	$\frac{9}{32}$ 0.0037	$\frac{1}{4}$ 0.0035	$\frac{7}{32}$ 0.0032
4	2 0.0276	$1\frac{11}{32}$ 0.0184	1 0.0138	$1\frac{1}{16}$ 0.0112	$\frac{21}{32}$ 0.0092	$\frac{9}{16}$ 0.0079	$\frac{1}{2}$ 0.0069	$\frac{7}{16}$ 0.0061	$\frac{13}{32}$ 0.0056	$\frac{11}{32}$ 0.0049	$\frac{11}{32}$ 0.0046	$\frac{5}{16}$ 0.0043
5	$2\frac{1}{2}$ 0.0345	$1\frac{21}{32}$ 0.0230	$1\frac{1}{4}$ 0.0172	1 0.0138	$\frac{27}{32}$ 0.0115	$\frac{23}{32}$ 0.0099	$\frac{5}{8}$ 0.0086	$\frac{9}{16}$ 0.0076	$\frac{1}{2}$ 0.0069	$\frac{7}{16}$ 0.0062	$\frac{13}{32}$ 0.0058	$\frac{3}{8}$ 0.0054
6	3 0.0414	2 0.0276	$1\frac{1}{2}$ 0.0207	$1\frac{3}{16}$ 0.0166	1 0.0138	$\frac{27}{32}$ 0.0118	$\frac{3}{4}$ 0.0103	$\frac{21}{32}$ 0.0092	$\frac{19}{32}$ 0.0083	$\frac{17}{32}$ 0.0075	$\frac{1}{2}$ 0.0069	$\frac{15}{32}$ 0.0064
7	$3\frac{1}{2}$ 0.0484	$2\frac{11}{32}$ 0.0323	$1\frac{3}{4}$ 0.0242	$1\frac{13}{32}$ 0.0194	$1\frac{5}{32}$ 0.0161	1 0.0138	$\frac{7}{8}$ 0.0121	$\frac{25}{32}$ 0.0108	$\frac{11}{16}$ 0.0097	$\frac{5}{8}$ 0.0088	$\frac{19}{32}$ 0.0081	$\frac{17}{32}$ 0.0074
8	4 0.0553	$2\frac{21}{32}$ 0.0369	2 0.0277	$1\frac{19}{32}$ 0.0221	$1\frac{11}{32}$ 0.0184	$1\frac{5}{32}$ 0.0158	1 0.0138	$\frac{7}{8}$ 0.0123	$\frac{13}{16}$ 0.0111	$\frac{23}{32}$ 0.0101	$\frac{21}{32}$ 0.0092	$\frac{5}{8}$ 0.0085
9	$4\frac{1}{2}$ 0.0622	3 0.0415	$2\frac{1}{4}$ 0.0311	$1\frac{13}{16}$ 0.0249	$1\frac{1}{2}$ 0.0207	$1\frac{9}{32}$ 0.0178	$1\frac{1}{8}$ 0.0156	1 0.0138	$\frac{29}{32}$ 0.0124	$\frac{13}{16}$ 0.0113	$\frac{3}{4}$ 0.0104	$\frac{11}{16}$ 0.0096
10	5 0.0691	$3\frac{11}{32}$ 0.0461	$2\frac{1}{2}$ 0.0345	2 0.0277	$1\frac{21}{32}$ 0.0230	$1\frac{7}{16}$ 0.0198	$1\frac{1}{4}$ 0.0173	$1\frac{3}{16}$ 0.0154	1 0.0138	$\frac{29}{32}$ 0.0126	$\frac{27}{32}$ 0.0115	$\frac{25}{32}$ 0.0106
11	$5\frac{1}{2}$ 0.0761	$3\frac{11}{16}$ 0.0507	$2\frac{3}{4}$ 0.0380	$2\frac{3}{16}$ 0.0304	$1\frac{27}{32}$ 0.0254	$1\frac{19}{32}$ 0.0219	$1\frac{3}{8}$ 0.0190	$1\frac{7}{32}$ 0.0169	$1\frac{3}{32}$ 0.0152	1 0.0138	$\frac{29}{32}$ 0.0127	$\frac{27}{32}$ 0.0117
12	6 0.0830	4 0.0553	3 0.0415	$2\frac{13}{32}$ 0.0332	2 0.0277	$1\frac{23}{32}$ 0.0237	$1\frac{1}{2}$ 0.0207	$1\frac{11}{32}$ 0.0184	$1\frac{1}{16}$ 0.0166	$1\frac{3}{32}$ 0.0151	1 0.0138	$\frac{15}{16}$ 0.0128

Overall
difference
in points

Total number of casts in strip

	14	15	16	17	18	19	20	21	22	23	24	25
$\frac{1}{2}$	$\frac{1}{32}$ 0.0005	$\frac{1}{32}$ 0.0005	$\frac{1}{32}$ 0.0004	$\frac{1}{32}$ 0.0004	$\frac{1}{32}$ 0.0004	$\frac{1}{32}$ 0.0004	$\frac{1}{32}$ 0.0004	$\frac{1}{32}$ 0.0003	$\frac{1}{32}$ 0.0003	$\frac{1}{32}$ 0.0003	$\frac{1}{32}$ 0.0003	$\frac{1}{32}$ 0.0003
1	$\frac{1}{16}$ 0.0010	$\frac{1}{16}$ 0.0009	$\frac{1}{16}$ 0.0009	$\frac{1}{16}$ 0.0008	$\frac{1}{16}$ 0.0008	$\frac{1}{16}$ 0.0007	$\frac{1}{16}$ 0.0007	$\frac{1}{32}$ 0.0006	$\frac{1}{32}$ 0.0006	$\frac{1}{32}$ 0.0006	$\frac{1}{32}$ 0.0006	$\frac{1}{32}$ 0.0006
2	$\frac{5}{32}$ 0.0020	$\frac{1}{8}$ 0.0019	$\frac{1}{8}$ 0.0017	$\frac{1}{8}$ 0.0016	$\frac{3}{32}$ 0.0015	$\frac{3}{32}$ 0.0014	$\frac{3}{32}$ 0.0014	$\frac{3}{32}$ 0.0013	$\frac{3}{32}$ 0.0012	$\frac{3}{32}$ 0.0012	$\frac{3}{32}$ 0.0011	$\frac{3}{32}$ 0.0011
3	$\frac{7}{32}$ 0.0030	$\frac{7}{32}$ 0.0028	$\frac{3}{16}$ 0.0026	$\frac{3}{16}$ 0.0025	$\frac{5}{32}$ 0.0023	$\frac{5}{32}$ 0.0022	$\frac{5}{32}$ 0.0021	$\frac{5}{32}$ 0.0020	$\frac{1}{8}$ 0.0019	$\frac{1}{8}$ 0.0018	$\frac{1}{8}$ 0.0017	$\frac{1}{8}$ 0.0017
4	$\frac{9}{32}$ 0.0039	$\frac{9}{32}$ 0.0037	$\frac{1}{4}$ 0.0035	$\frac{1}{4}$ 0.0033	$\frac{7}{32}$ 0.0031	$\frac{7}{32}$ 0.0029	$\frac{3}{16}$ 0.0027	$\frac{3}{16}$ 0.0026	$\frac{3}{16}$ 0.0025	$\frac{3}{16}$ 0.0024	$\frac{5}{32}$ 0.0023	$\frac{5}{32}$ 0.0022
5	$\frac{11}{32}$ 0.0049	$\frac{11}{32}$ 0.0046	$\frac{5}{16}$ 0.0043	$\frac{9}{32}$ 0.0041	$\frac{9}{32}$ 0.0038	$\frac{1}{4}$ 0.0036	$\frac{1}{4}$ 0.0034	$\frac{1}{4}$ 0.0033	$\frac{7}{32}$ 0.0031	$\frac{7}{32}$ 0.0030	$\frac{7}{32}$ 0.0028	$\frac{7}{32}$ 0.0028
6	$\frac{7}{16}$ 0.0059	$\frac{13}{32}$ 0.0055	$\frac{3}{8}$ 0.0052	$\frac{11}{32}$ 0.0049	$\frac{11}{32}$ 0.0046	$\frac{5}{16}$ 0.0043	$\frac{9}{32}$ 0.0041	$\frac{9}{32}$ 0.0039	$\frac{9}{32}$ 0.0038	$\frac{1}{4}$ 0.0036	$\frac{1}{4}$ 0.0034	$\frac{1}{4}$ 0.0033
7	$\frac{1}{2}$ 0.0069	$\frac{15}{32}$ 0.0065	$\frac{7}{16}$ 0.0061	$\frac{13}{32}$ 0.0057	$\frac{13}{32}$ 0.0054	$\frac{3}{8}$ 0.0051	$\frac{11}{32}$ 0.0048	$\frac{11}{32}$ 0.0046	$\frac{5}{16}$ 0.0044	$\frac{5}{16}$ 0.0042	$\frac{9}{32}$ 0.0040	$\frac{9}{32}$ 0.0039
8	$\frac{9}{16}$ 0.0079	$\frac{17}{32}$ 0.0074	$\frac{1}{2}$ 0.0069	$\frac{15}{32}$ 0.0065	$\frac{7}{16}$ 0.0061	$\frac{13}{32}$ 0.0058	$\frac{13}{32}$ 0.0055	$\frac{3}{8}$ 0.0053	$\frac{3}{8}$ 0.0052	$\frac{11}{32}$ 0.0048	$\frac{11}{32}$ 0.0046	$\frac{5}{16}$ 0.0044
9	$\frac{21}{32}$ 0.0089	$\frac{19}{32}$ 0.0083	$\frac{9}{16}$ 0.0078	$\frac{17}{32}$ 0.0073	$\frac{1}{2}$ 0.0069	$\frac{15}{32}$ 0.0065	$\frac{7}{16}$ 0.0062	$\frac{7}{16}$ 0.0059	$\frac{13}{32}$ 0.0056	$\frac{13}{32}$ 0.0054	$\frac{3}{8}$ 0.0052	$\frac{3}{8}$ 0.0050
10	$\frac{23}{32}$ 0.0099	$\frac{21}{32}$ 0.0092	$\frac{5}{8}$ 0.0086	$\frac{19}{32}$ 0.0081	$\frac{9}{16}$ 0.0077	$\frac{17}{32}$ 0.0073	$\frac{1}{2}$ 0.0069	$\frac{15}{32}$ 0.0066	$\frac{15}{32}$ 0.0063	$\frac{7}{16}$ 0.0060	$\frac{13}{32}$ 0.0058	$\frac{13}{32}$ 0.0055
11	$\frac{25}{32}$ 0.0109	$\frac{23}{32}$ 0.0101	$\frac{11}{16}$ 0.0095	$\frac{21}{32}$ 0.0089	$\frac{5}{8}$ 0.0085	$\frac{19}{32}$ 0.0080	$\frac{9}{16}$ 0.0076	$\frac{17}{32}$ 0.0072	$\frac{1}{2}$ 0.0069	$\frac{15}{32}$ 0.0066	$\frac{7}{16}$ 0.0063	$\frac{7}{16}$ 0.0061
12	$\frac{27}{32}$ 0.0119	$\frac{13}{16}$ 0.0111	$\frac{3}{4}$ 0.0104	$\frac{23}{32}$ 0.0098	$\frac{21}{32}$ 0.0092	$\frac{5}{8}$ 0.0087	$\frac{19}{32}$ 0.0083	$\frac{9}{16}$ 0.0079	$\frac{17}{32}$ 0.0075	$\frac{17}{32}$ 0.0072	$\frac{1}{2}$ 0.0069	$\frac{15}{32}$ 0.0066

Product information table

For 'Monotype' Super Casters equipped with Varigear

	Leads and rules				Leads, rules and borders				
	1pt	1½pt	2pt	3pt	4pt	6pt	8pt	12pt	18pt
Speed r.p.m.	130	125	100	85	70	55	40	25	20
Temperature °F	720	700	675	625	700	650	650	625	625
Temperature °C	382	371	357	329	371	343	343	329	329
Water flow	small	small	small	small	medium	medium	medium	medium	medium
Cam lever extension	12/1/1½	12/1/1½	12/2/4	12/2/4	12/2/4	12/6	12/6	12/12	12/18
Mould blade connecting tube	leads	leads	leads	leads	leads	leads	leads	leads	leads
Fulcrum eccentric pin	1-3L/R	1-3L/R	1-3L/R	1-3L/R	42-72	42-72	42-72	42-72	42-72
Plunger spring pressure	zero	zero	zero	zero	slight	slight	slight	slight	fair
Stop lever handle	leads	leads	leads	leads	leads	leads	leads	leads	leads
Latch trip plates (upper)	—	—	—	—	6	4	4	4	2
Spring rod stop plates (lower)	—	—	—	—	1	2	2	3	4
Latch spring	out	out	out	out	in	in	in	in	in
Nozzle number	10	10	10	10	11	11	11	8	8
Clearing drill diam. (top)	$\frac{1}{16}$ "	$\frac{1}{16}$ "	$\frac{1}{16}$ "	$\frac{1}{16}$ "	0-082	0-082	0-082	0-120	0-120
Clearing drill diam. (bottom)	0-180	0-180	0-180	0-180	0-152	0-152	0-152	0-120	0-120
Nozzle seating and timing	out	out	out	out	out	out	out	out	in
Pump body	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	1¼"	1¼"
Piston required $\frac{7}{8}$ "	long	long	long	long	long	short	short	—	—
Pump body lifting spring plate hole	bottom	bottom	bottom	bottom	top	top	top	top	top
Duplex spring compression	2¾"	2½"	1½"	1½"	2"	2"	2"	2"	2"
Air	no	no	no	no	no	no	no	no	no
Type channel block	no	no	no	no	no	no	no	no	no
Matrix head locating key	—	—	—	—	—	—	—	—	—
Mould water way	— leads, rules & furniture —				— leads, rules & furniture —				

The value of some of the information in this table represents only recommended averages: variations in local conditions and requirements significantly affect the factors upon which it is based.

For 'Monotype' Super Casters equipped with Varigear

	†Duplex			†Triplex	†Composition type				
	14pt	16pt	18pt		24pt	6,7,8pt	9,10,11pt	12pt	13pt
Speed r.p.m.	130	125	110	90	160	150	130	130	130
Temperature °F	700	700	700	700	700	700	675	675	675
Temperature °C	371	371	371	371	371	371	357	357	357
Water flow	medium	medium	medium	medium	small	small	small	medium	medium
Cam lever extension	24	24	24	24	12	12	12	12	12
Mould blade connecting tube	42	42	42	42	42	42	42	42	42
Fulcrum eccentric pin	5/36	5/36	5/36	5/36	5/36	5/36	5/36	5/36	5/36
Plunger spring pressure	slight	slight	slight	slight	zero	zero	zero	zero	slight
Stop lever handle	16	16	16	16	16	16	16	16	16
Latch trip plates (upper)	6	6	6	6	—	—	—	—	—
Spring rod stop plates (lower)	1	1	1	1	—	—	—	—	—
Latch spring	in	in	in	in	out	out	out	out	out
Nozzle number	2	2	2	2	16	1	1	1	1
Clearing drill diam. (top)	0.120	0.120	0.120	0.120	0.062	0.062	0.062	0.062	0.062
Clearing drill diam. (bottom)	0.120	0.120	0.120	0.120	0.093	0.120	0.120	0.120	0.120
Nozzle seating and timing	out	out	out	out	out	out	out	out	out
Pump body	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "
Piston required $\frac{7}{8}$ "	short	short	short	short	long	long	long	long	long
Pump body lifting spring plate hole	top	top	top	top	bottom	bottom	bottom	bottom	bottom
Duplex spring compression	$\frac{3}{4}$ "	$\frac{3}{4}$ "	$\frac{3}{4}$ "	1"	nil	$\frac{1}{4}$ "	$\frac{1}{2}$ "	$\frac{1}{2}$ "	$\frac{1}{2}$ "
Air	yes	yes	yes	yes	yes	yes	yes	yes	yes
Type channel block	14-72 solid type			14-72 solid type	5-13	5-13	5-13	5-13	5-13
Matrix head locating key	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36
Mould water way	AB	AB	AB	AB	AB	AB	AB	AB	AB

†Based on the half em body

The value of some of the information in this table represents only recommended averages: variations in local conditions and requirements significantly affect the factors upon which it is based.

Product information table (continued)

For 'Monotype' Super Casters equipped with Varigear

	†Display type										
	14pt	16pt	18pt	24pt	28pt	30pt	36pt	42pt	48pt	60pt	72pt
Speed r.p.m.	125	110	100	55	45	35	25	20	15	10	8
Temperature °F	670	650	645	640	640	635	630	625	615	610	610
Temperature °C	354	343	340	337	337	335	332	329	323	321	321
Water flow	medium	medium	medium	medium	medium	medium	medium	large	large	large	large
Cam lever extension	24	24	24	24	24	36	36	48	48	60	72
Mould blade connecting tube	42	42	42	42	42	42	42	— according to set —			
Fulcrum eccentric pin	5/36	5/36	5/36	5/36	5/36	5/36	5/36	42/72	42/72	42/72	42/72
Plunger spring pressure	slight	slight	slight	slight	slight	slight	slight	fair	fair	fair	fair
Stop lever handle	16	16	16	16	16	16	16	16	16	16	16
Latch trip plates (upper)	6	6	6	6	6	6	5	6	4	3	3
Spring rod stop plates (lower)	1	1	1	1	1	1	2	2	2	3	4
Latch spring	in	in	in	in	in	in	in	in	in	in	in
Nozzle number	2	2	2	2	2	2	2	5‡	5‡	5‡	5‡
Clearing drill diam. (top)	0-120	0-120	0-120	0-120	0-120	0-120	0-120	0-213	0-213	0-213	0-213
Clearing drill diam. (bottom)	0-120	0-120	0-120	0-120	0-120	0-120	0-120	0-302	0-302	0-302	0-302
Nozzle seating and timing	out	out	out	out	out	out	out	in	in	in	in
Pump body	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	1 $\frac{1}{4}$ "	1 $\frac{1}{2}$ "	1 $\frac{1}{2}$ "	1 $\frac{1}{2}$ "
Piston required $\frac{7}{8}$ "	short	short	short	short	short	short	short	—	—	—	—
Pump body lifting spring plate hole	top	top	top	top	top	top	top	top	top	top	top
Duplex spring compression	$\frac{3}{4}$ "	$\frac{3}{4}$ "	$\frac{3}{4}$ "	1"	1"	1 $\frac{1}{4}$ "	1 $\frac{1}{2}$ "	2"	2"	2 $\frac{1}{4}$ "	3"
Air	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes
Type channel block	14-72 solid type						40-72 light type				
Matrix head locating key	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	42-72	42-72	42-72	42-72
Mould water way	14-36	14-36	14-36	14-36	14-36	14-36	14-36	42-72	42-72	42-72	42-72

†Based on the half em body

‡For thin spaces use No. 6 Nozzle

The value of some of the information in this table represents only recommended averages; variations in local conditions and requirements significantly affect the factors upon which it is based.

For 'Monotype' Super Casters equipped with Varigear

	Dashes 16 em (15 cicero ems)				Furniture				
	4pt	6pt	12pt	18pt	24pt	36pt	48pt	60pt	72pt
Speed r.p.m.	40	30	15	8	12	10	10	9	8
Temperature °F	675	625	600	600	630	630	630	630	630
Temperature °C	357	329	315	315	332	332	332	332	332
Water flow	medium	medium	medium	medium	large	large	large	large	large
Cam lever extension	12/2/4	12/6	12/12	12/18	12/12	12/12	12/12	12/12	12/12
Mould blade connecting tube	dashes	dashes	dashes	dashes	furniture	furniture	furniture	furniture	furniture
Fulcrum eccentric pin	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72
Plunger spring pressure	slight	slight	slight	fair	fair	fair	fair	fair	fair
Stop lever handle	16	16	16	16	13*	13*	13*	13*	13*
Latch trip plates (upper)	6	4	4	2	4	4	3	3	2
Spring rod stop plates (lower)	1	2	3	4	3	3	4	4	4
Latch spring	in	in	in	in	in	in	in	in	in
Nozzle number	11	11	8	8	5	5	5	5	5
Clearing drill diam. (top)	0-082	0-082	0-082	0-120	0-213	0-213	0-213	0-213	0-213
Clearing drill diam. (bottom)	0-152	0-152	0-152	0-120	0-302	0-302	0-302	0-302	0-302
Nozzle seating and timing	out	out	in	in	in	in	in	in	in
Pump body	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$1\frac{1}{4}$ "	$1\frac{1}{4}$ "	$1\frac{1}{2}$ "	$1\frac{1}{4}$ "	$1\frac{1}{4}$ "	$1\frac{1}{4}$ "	$1\frac{1}{4}$ "
Piston required $\frac{7}{8}$ "	short	short	—	—	—	—	—	—	—
Pump body lifting spring plate hole	top	top	top	top	top	top	top	top	top
Duplex spring compression	2"	2"	2"	2"	$2\frac{1}{4}$ "	$2\frac{1}{4}$ "	$2\frac{1}{4}$ "	$2\frac{1}{4}$ "	$2\frac{1}{4}$ "
Air	no	no	no	no	no	no	no	no	no
Type channel block	no	no	no	no	no	no	no	no	no
Matrix head locating key	—	—	—	—	—	—	—	—	—
Mould water way	— leads, rules & furniture —				— leads, rules & furniture —				

*When using predetermined length furniture mould place stop lever handle at top position

The value of some of the information in this table represents only recommended averages: variations in local conditions and requirements significantly affect the factors upon which it is based.

Product information table (continued)

For 'Monotype' Super Casters equipped with Varigear

	Foundry furniture (top section)				Mounting material			Two-way mounting material
	36pt	48pt	60pt	72pt	24pt	36pt	48pt	
Speed r.p.m.	12	12	12	10	12	10	10	5½
Temperature °F	630	630	630	630	630	630	630	585
Temperature °C	332	332	332	332	332	332	332	307
Water flow	large	large	large	large	large	large	large	large
Cam lever extension	12/12	12/12	12/12	12/12	12/12	12/12	12/12	12/12
Mould blade connecting tube	furniture	furniture	furniture	furniture	furniture	furniture	furniture	furniture
Fulcrum eccentric pin	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72
Plunger spring pressure	fair	fair	fair	fair	fair	fair	fair	fair
Stop lever handle	13*	13*	13*	13*	13*	13*	13*	13*
Latch trip plates (upper)	2	2	2	2	2	2	2	1
Spring rod stop plates (lower)	4	4	4	4	4	4	4	4
Latch spring	in	in	in	in	in	in	in	in
Nozzle number	5	5	5	5	5	5	5	5
Clearing drill diam. (top)	0.213	0.213	0.213	0.213	0.213	0.213	0.213	0.213
Clearing drill diam. (bottom)	0.302	0.302	0.302	0.302	0.302	0.302	0.302	0.302
Nozzle seating and timing	in	in	in	in	in	in	in	in
Pump body	1¼"	1¼"	1¼"	1¼"	1¼"	1¼"	1¼"	1¼"
Piston required $\frac{7}{8}$ "	—	—	—	—	—	—	—	—
Pump body lifting spring plate hole	top	top	top	top	top	top	top	top
Duplex spring compression	2¼"	2¼"	2¼"	2¼"	2¼"	2¼"	2¼"	3¼"
Air	no	no	no	no	no	no	no	no
Type channel block	no	no	no	no	no	no	no	no
Matrix head locating key	—	—	—	—	—	—	—	—
Mould water way	— leads, rules & furniture —				— leads, rules & furniture —			

*When using predetermined length furniture mould place stop lever handle at top position

The value of some of the information in this table represents only recommended averages: variations in local conditions and requirements significantly affect the factors upon which it is based.

For 'Monotype' Super Casters equipped with Varigear

	Quotations											
	6×6ems	6×5ems	6×4ems	6×3ems	6×2ems	5×5ems	5×4ems	5×3ems	5×2ems	4×4ems	4×3ems	4×2ems
Speed r.p.m.	4	5	6	8	8	5	6	8	10	8	10	12
Temperature °F	600	600	600	600	600	600	600	600	600	600	600	600
Temperature °C	315	315	315	315	315	315	315	315	315	315	315	315
Water flow	large	large	large	large	large	large	large	large	large	large	large	large
Cam lever extension	72	72	72	72	72	60	60	60	60	48	48	48
Mould blade connecting tube	72-90	48-60	48-60	42	42	48-60	48-60	42	42	48-60	42	42
Fulcrum eccentric pin	42-72	42-72	42-72	5-36	5-36	42-72	42-72	5-36	5-36	42-72	5-36	5-36
Plunger spring pressure	fair	fair	fair	fair	slight	fair	fair	fair	slight	fair	fair	slight
Stop lever handle	16	16	16	16	16	16	16	16	16	16	16	16
Latch trip plates (upper)	3	4	3	4	4	3	4	4	4	4	5	6
Spring rod stop plates (lower)	4	4	3	3	2	4	3	2	2	1	1	1
Latch spring	in	in	in	in	in	in	in	in	in	in	in	in
Nozzle number	5	5	6	6	6	6	6	6	6	4	4	4
Clearing drill diam. (top)	0.213	0.213	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.213	0.213	0.213
Clearing drill diam. (bottom)	0.302	0.302	0.120	0.120	0.120	0.120	0.120	0.120	0.120	0.213	0.213	0.213
Nozzle seating and timing	in	in	in	in	in	in	in	in	in	in	in	in
Pump body	1½"	1¾"	1¼"	1¾"	1¾"	1¼"	1¾"	1¾"	1¼"	7⁄8"	7⁄8"	7⁄8"
Piston required 7⁄8"	—	—	—	—	—	—	—	—	—	short	short	short
Pump body lifting spring plate hole	top	top	top	top	top	top	top	top	top	top	top	top
Duplex spring compression	2½"	2¼"	2½"	2¼"	2"	2½"	2½"	2¼"	2"	1¾"	1½"	1½"
Air	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes	yes
Type channel block	36-72	36-72	36-72	36-72	36-72	36-72	36-72	36-72	36-72	36-72	36-72	36-72
Matrix head locating key	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72
Mould water way	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72	42-72

The value of some of the information in this table represents only recommended averages: variations in local conditions and requirements significantly affect the factors upon which it is based.

Product information table (continued)

For 'Monotype' Super Casters equipped with Varigear

	Quad and space									
	5, 6pt§	7, 8pt§	9, 10pt§	11, 12pt§	13, 14pt§	5, 6pt††	7, 8pt††	9, 10pt††	11, 12pt††	13, 14pt††
Speed r.p.m.	150	145	140	125	110	75	70	55	45	35
Temperature °F	700	700	700	700	700	700	700	700	675	675
Temperature °C	371	371	371	371	371	371	371	371	357	357
Water flow	medium	medium	medium	medium	medium	medium	medium	medium	medium	medium
Cam lever extension	12	12	12	12	12	12	12	12	12	24
Mould blade connecting tube	42	42	42	42	42	42	42	42	42	42
Fulcrum eccentric pin	5-36	5-36	5-36	5-36	5-36	5-36	5-36	5-36	5-36	5-36
Plunger spring pressure	zero	zero	zero	zero	zero	zero	zero	zero	zero	zero
Stop lever handle	16	16	16	16	16	16	16	16	16	16
Latch trip plates (upper)	—	—	—	—	—	—	—	—	6	6
Spring rod stop plates (lower)	—	—	—	—	—	—	—	—	1	1
Latch spring	out	out	out	out	out	out	out	out	in	in
Nozzle number	16	16	1	1	1	1	1	1	1	1
Clearing drill diam. (top)	0-062	0-062	0-062	0-062	0-062	0-062	0-062	0-062	0-062	0-062
Clearing drill diam. (bottom)	0-093	0-093	0-120	0-120	0-120	0-120	0-120	0-120	0-120	0-120
Nozzle seating and timing	out	out	out	out	out	out	out	out	out	out
Pump body	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "
Piston required $\frac{7}{8}$ "	short	short	short	short	short	short	short	short	short	short
Pump body lifting spring plate hole	bottom	bottom	bottom	bottom	bottom	bottom	bottom	bottom	bottom	bottom
Duplex spring compression	nil	nil	$\frac{1}{4}$ "	$\frac{1}{4}$ "	$\frac{1}{4}$ "	$\frac{1}{4}$ "	$\frac{1}{2}$ "	$\frac{1}{2}$ "	$\frac{1}{2}$ "	$\frac{1}{2}$ "
Air	no	no	no	no	no	no	no	no	no	no
Type channel block	5-13	5-13	5-13	5-13	5-13	5-13	5-13	5-13	5-13	5-13
Matrix head locating key	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36
Mould water way	AB	AB	AB	AB	AB	AB	AB	AB	AB	AB

§Quad

††Maximum opening

The value of some of the information in this table represents only recommended averages: variations in local conditions and requirements significantly affect the factors upon which it is based.

For 'Monotype' Super Casters equipped with Varigear

	†Palace Script and Italic					
	14pt	18pt	24pt	30pt	36pt	42pt
Speed r.p.m.	95	75	45	25	18	15
Temperature °F	675	670	660	660	650	640
Temperature °C	357	354	349	349	343	337
Water flow	medium	medium	medium	medium	medium	large
Cam lever extension	24	24	24	36	36	48
Mould blade connecting tube	48-60	48-60	48-60	48-60	48-60	48-60††
Fulcrum eccentric pin	5-36	5-36	5-36	5-36	5-36	42-72
Plunger spring pressure	slight	slight	slight	slight	slight	fair
Stop lever handle	16	16	16	16	16	16
Latch trip plates (upper)	6	6	6	6	5	5
Spring rod stop plates (lower)	1	1	1	1	2	2
Latch spring	in	in	in	in	in	in
Nozzle number	2	2	2	2	2	2
Clearing drill diam. (top)	0-120	0-120	0-120	0-120	0-120	0-120
Clearing drill diam. (bottom)	0-120	0-120	0-120	0-120	0-120	0-120
Nozzle seating and timing	out	out	out	out	in	in
Pump body	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "	$\frac{7}{8}$ "
Piston required $\frac{7}{8}$ "	short	short	short	short	short	short
Pump body lifting spring plate hole	top	top	top	top	top	top
Duplex spring compression	$\frac{3}{4}$ "	$\frac{3}{4}$ "	$\frac{3}{4}$ "	1"	1 $\frac{1}{4}$ "	1 $\frac{1}{2}$ "
Air	no	no	no	no	no	no
Type channel block	14-72	14-72	14-72	14-72	14-72	42-72
Matrix head locating key	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36	5 $\frac{1}{2}$ -36
Mould water way	14-36	14-36	14-36	14-36	14-36	14-36

†Based on the half em body

††72pt hole for blade openings greater than 0-5"

The value of some of the information in this table represents only recommended averages: variations in local conditions and requirements significantly affect the factors upon which it is based.

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GLOSSARY

The following brief glossary has been compiled to explain the meaning of some unfamiliar words that you may come across in this book, some of which are peculiar to the printing industry.

Capitals	Large form of characters, (sometimes referred to as <i>upper case</i>), technically described as majuscule.
Character	Any letter, figure or punctuation mark, including special symbols such as those used in cartography, mathematics, etc.
Cicero	Traditional printer's unit of measure, commonly used in Europe. 1 cicero = 0.1776 in (4.511 mm) = 12 Didot points.
Clumps	Metal spacing material 6 points and 12 points in thickness.
Composition	Setting up matter, with spaces between the words.
Copy	All manuscript, and other material, supplied to a printer for typesetting.
Didot	A unit of linear measure. It is one twelfth part of a cicero and measures 0.0148 in (0.376 mm).
Electro (abbr.)	A hard-wearing printing plate made by depositing a film of copper electrolytically on a wax mould taken from type or an original plate. The copper shell is filled with a lead alloy.
Em	A standard of typographic measurement based on a quad 12 points deep by 12 points wide (0.166 in × 0.166 in), approximately six quads to the inch. When the term refers to overall measure, a 12-set em (1 pica) is inferred.
En	Half an em.
Fount	The complete assortment of type characters of the same design and size. (Generally pronounced <i>font</i> .)
Full point	A full stop (punctuation mark).
Furniture	Spacing material of less than type height, used in making margins, etc. for a printed sheet.
Galley	A metal tray on which type is made up, or stored.
Justification	The spacing of words to a given width of line when setting type matter. Purpose: to align type matter at the right-hand margin of a page.
Leaders	A sequence of dots, or dashes, used to direct the eye across the printed page. Generally appearing two, three or more to the em.
Leads	Strips of type alloy (of less than type height) used to increase space between lines of type.
Ligature	Two or more letters joined together, and cast on one body.
Line of a character	An imaginary base-line, running setwise, on (or about) which the character is positioned.
Lower case	The small form of letters, technically described as miniscule where capitals are referred to as majuscule.
Matrix	A metal die from which a single type is cast.

Glossary (*continued*)

Matrix line	The measurement from the line of a character to the opposite edge of a matrix. This applies to 0.2 in × 0.2 in matrices, and the line for each point size in a typeface is shown on the specimen sheets of 'Monotype' typefaces.
Mould	The cavity into which molten metal is injected to produce the body or shank of the type. The face of the type is produced by a matrix (q.v.) which is individual to the character, and which acts as a temporary part of the mould.
Pica	The traditional printer's unit of measure, it is equal to 12 points and measures 0.166 in. Line-lengths are normally expressed as so many picas long.
Point	A unit of measurement for type body size. Seventy-two points very approximately equal one inch, and one point measures 0.0138333 in. Abbreviation <i>pt.</i>
Quads	Blank type (of less than type height) for use as spaces.
Quotations	Large metal spaces ranging in size from 2 × 4 ems to 6 × 6 ems. They are usually hollow, and are used for filling blank areas in pages or formes.
Rules	Strips of brass or type alloy (of type height) cast in various point-sizes and lengths.
Set (set width)	The measurement, in points, of the width of an <i>em</i> quad.
Setwise (direction)	Horizontally, across the text.
Small capitals	Characters which have the same form as capitals, but are smaller, being produced to the same x-height as the lower-case characters.
Stereo (abbr.)	A lead-based metal plate cast from a papier-mâché matrix (flong) produced from a type forme or original plate.
Tie-up slugs	Metal strips of less than type height, measuring 12 points at top and bottom, but deeply recessed on one side. Placed around the type page, they provide an unbroken external recess in which the pagecord lies without projecting beyond the 12-point metal.
Typeface	A type design which is given a name and series number – e.g. Times New Roman, Series 327.
Type line	The measurement from the line of the character to the top of the type body. This applies to type larger than 14 point, or 14-point type from large-type composition matrices.
Units	A unit of set is a variable dimension, dependent on the set of the fount. The basic unit of set is one eighteenth of 1 point = 0.0007685 in, a figure that is used only as a foundation for calculations. One unit of an 8-set fount is therefore 8 × 0.0007685 in = 0.006148 in. When referring to units, it is essential to stipulate <i>basic units</i> or the set of the fount concerned – the expression <i>10 units</i> (unspecified) has no meaning, but <i>10 units of 6 set</i> (for example) is 0.04611. Note that 6 units of 10 set have the same total width as 10 units of 6 set, as, in each case, 60 basic units are required.
x-height	The height of the lower-case alphabet excluding ascenders and descenders, with x as the standard in any given fount.

FURTHER READING

History

A Chronology of Printing by *Colin Clair*
Cassell

Five Hundred Years of Printing by *S. H. Steinberg*
Penguin

Printing Types: their history, forms and use by *Daniel B. Updike*
Oxford University Press

The Printed Book by *Harry G. Aldis*
Third edition revised by John Carter and Brooke Crutchley
Cambridge University Press

Composing and Typography

Advanced Typography for Students by *E. G. Shepherd, FRSA*
Macdonald and Evans

An Encyclopaedia of Type Faces by *W. Turner Berry, A. F. Johnson and W. P. Jaspert*
Blandford Press

Compositors' Equipment by *Charles L. Pickering*
Pitman

Compositors' Work by *Charles L. Pickering*
Pitman

Compositors' Work in Printing by *H. W. Larken*
Staples

Factors in the Choice of Type Faces by *Geoffrey Dowding*
Wace

Finer Points in the Spacing and Arrangement of Type
by *Geoffrey Dowding*
Wace

Introduction to Typography by *Oliver Simon*
Penguin

Letterpress: Composition and Machine Work by *C. A. Hurst and F. R. Lawrence*
Benn

Methods of Book Design by *Hugh Williamson*
Oxford University Press

Modern Printing by *John Southward* (Volume 1)
Charles Skilton Ltd

Typography for Students by *E. G. Shepherd, FRSA*
Macdonald and Evans

Further reading (*continued*)

Style

Authors' and Printers' Dictionary by *F. Howard Collins*
Oxford University Press

Concise Oxford Dictionary
Oxford University Press

Division of Words in Foreign Languages
The Monotype Corporation Ltd

Modern English Usage by *H. W. Fowler*
Oxford University Press

Printed English by *Henry Jacob*
Sylvan Press

Printing Style by *James Jarrett*
Allen and Unwin

Punctuation by *G. V. Carey* with an appendix by *P. G. Burbidge*
Cambridge University Press

**Rules for Compositors and Readers at
the University Press, Oxford** by *Horace Hart*
Oxford University Press

Style for Print and Proof Correction by *R. A. Hewitt*
Blandford Press

'Monotype' Machines

(The following are obtainable from The Monotype Corporation Ltd)

*Attachments Booklet; A 'Monotype' Composing Machine Described;
'Monotype' Keyboard Manual; Book of Information;
'Monotype' Composition Caster Manual*

Type Metals

An Introduction to Science for Printers by *G. R. Marshall*
Heinemann

Efficient Remelting
Fry's Metal Foundries Ltd

Printing Metals
Fry's Metal Foundries Ltd

Printing Metals: their production, nature and use
Capper Pass, and Son Ltd

Organisation

Organisation and Management: Works by *F. Shackleton*
Pitman

Organisation and Management: Office by *F. Shackleton*
Pitman